# DEWALT.

TO:				
PROJECT:				
PROJECT LOCATIO	N:			
SPECIFIED ITEM:				
Section	Page	Paragraph	Description	
PRODUCT SI	IRMIT TAL / SURSI	TITUTION REQUESTED:		

The attached submittal package includes the product description, specifications, drawings, and performance data for use in the evaluation of the request.

SUBMITTED B	γ:	
Name:		Signature:
Company:		
Address:		
Date:	Telephone:	Fax:
FOR USE BY 1	THE ARCHITECT AND/OR ENGI	IEER
Approved	Approved as Noted	Not Approved
(If not approved, pleas	se briefly explain why the product was not ac	epted.)
By:		Date:

Remarks:



#### DEWALT® Hangermate(R)+ Anchors & Accessories Submittal Section:

#### **Competitive Comparisons:**

- DEWALT® Hangermate(R)+ Anchors & Accessories vs. ITW\* SAMMYS®
- DEWALT® Hangermate(R)+ Anchors & Accessories vs. HILTI\* KH-EZ I VS. SIMPSON\* TITEN HD ROD HANGER
- DEWALT® Hangermate(R)+ Anchors & Accessories vs. HILTI\* KH-EZ I

#### **Product Pages:**

- General Information
- Installation Instructions
- Design Tables
- Ordering Information

#### **Code Reports & Agency Listings:**

- ICC-ES Approval: ESR-3889 (Cracked & Uncracked Concrete)



Offline version available for download at <u>www.dewaltdesignassist.com</u>.

DEWALT developed the DEWALT Design Assist (DDA) anchor software to enable users to input technical data into a dynamic model environment-to visualize, consider, and specify anchors in today's changing engineering climate.

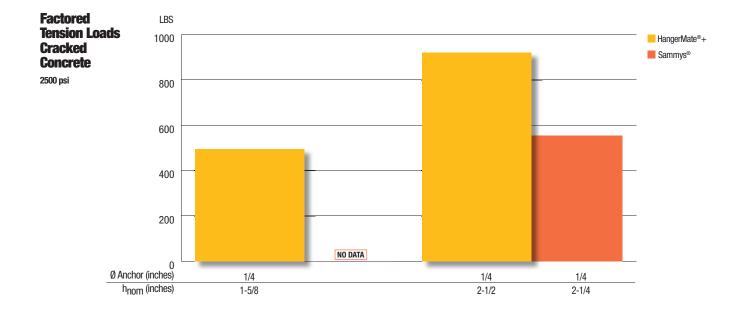
For a demonstration of the latest version of PDA, contact us at <u>anchors@DEWALT.com</u>

# **COMPETITIVE COMPARISON**

### HANGERMATE®+ VS. ITW\* SAMMYS®

#### **Product Comparison**

Product comparison		
Product Name	HangerMate®+	Sammys®
Company	DeWALT	ITW*
Description	Carbon Steel Screw Anchor	Carbon Steel Screw Anchor
Size Range (inch)	1/4, (1/4 and 3/8 Head)	1/4 (3/8 Head)
ICC-ES ESR (concrete)	ESR-3889	ESR-3699
Revision Date	2016 Nov	2016 March
Cracked Concrete	Yes	Yes
Seismic	Yes	Yes
Concrete-filled Steel Deck	Yes	No
* ITW Red Head and Sammys are registered trademark of Illin	ois Tool Works, Inc.	



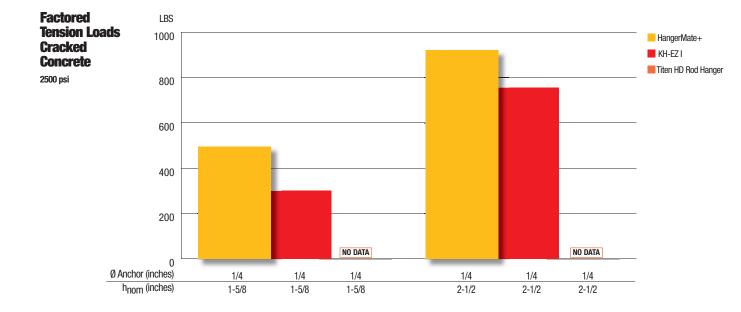


# **COMPETITIVE COMPARISON**

#### HANGERMATE®+ VS. HILTI\* KH-EZ I VS. SIMPSON\* TITEN HD ROD HANGER

#### **Product Comparison**

i rodučt obinparišon							
Product Name	HangerMate+	KH-EZ I	Titen HD Rod Hanger				
Company	DeWALT	Hilti*	Simpson*				
Description	Carbon Steel Screw Anchor	Carbon Steel Screw Anchor	Carbon Steel Screw Anchor				
Size Range (inch)	1/4 (1/4" & 3/8" Head)	1/4 (1/4" & 3/8" Head)	No 1/4 Shank Approved				
ICC-ES ESR (concrete)	ESR-3889	ESR-3027	ESR-2713				
Revision Date	2016 Nov	2015 Dec	2016 Sept				
Cracked Concrete	Yes	Yes	No				
Seismic	Yes	Yes	No				
Concrete-filled Steel Deck	Yes	Yes	No				
* Hilti is a registered trademark of Hilti Corpora	ation * Simpson and Titen HD Rod Hanger are registered tradem	arks of Simpson Strong-Tie Company Inc.					

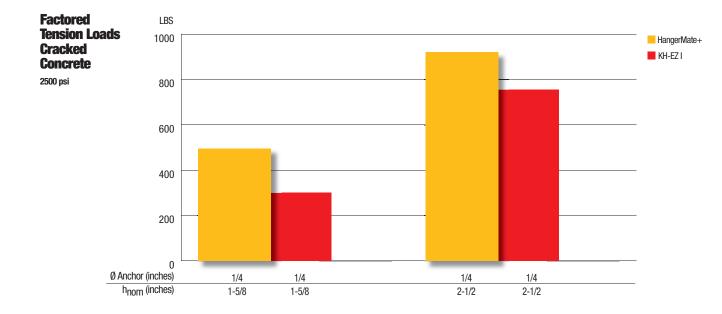


# **COMPETITIVE COMPARISON**

#### HANGERMATE®+ VS. HILTI<sup>\*</sup> KH-EZ I

### **Product Comparison**

FI VUULL UVIIIPAI ISVII	r rouuct companyon								
Product Name	HangerMate+	KH-EZ I							
Company	DeWALT	Hilti*							
Description	Carbon Steel Screw Anchor	Carbon Steel Screw Anchor							
Size Range (inch)	1/4 (1/4" & 3/8" Head)	1/4 (1/4" & 3/8" Head)							
ICC-ES ESR (concrete)	ESR-3889	ESR-3027							
Revision Date	2016 Nov	2015 Dec							
Cracked Concrete	Yes	Yes							
Seismic	Yes	Yes							
Concrete-filled Steel Deck	Yes	Yes							
* Hilti is a registered trademark of Hilti Corporation									



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Rod Hanging Anchor

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#### **GENERAL INFORMATION**

## CONCRETE HANGERMATE®+

Rod Hanging Anchor

#### **PRODUCT DESCRIPTION**

The Hangermate®+ concrete screw is a one piece, steel anchor designed for rod hanging applications such as fire protection systems, ventilation systems, electrical conduit, pipe hanging and cable trays. Tested and qualified for use in cracked concrete and seismic conditions. The concrete Hangermate® + requires a 1/4" ANSI masonry bit for installation, accepts 1/4" and 3/8" diameter threaded rods and is also available in a 3/8" male thread version.

Suspended Ceilings

Overhead Utilities

Lighting Systems

#### **GENERAL APPLICATIONS AND**

- Fire Sprinkler Pipes
- Ventilation Systems
- Cable Travs

#### FEATURES AND BENEFITS

- + Installs with standard 1/4-inch ANSI drill bit
- + Faster installation resulting in labor savings
- + Patented thread design offers low installation torque
- + Tough threads for tapping high strength concrete

#### **APPROVALS AND LISTINGS**

- International Code Council, Evaluation Service (ICC-ES). ESR-3889 code compliant with the 2015 IBC/IRC, 2012 IBC/IRC, and 2009 IBC/IRC.
- FM Approvals (FM) (see listing for applicable sizes and types).
- Tested in accordance with ACI 355.2/ASTM E 488 and ICC-ES AC193 for use in structural concrete under the design provisions of ACI 318-14, Chapter 17 and ACI-318-11/08 Appendix D.
- Evaluated and qualified by an accredited independent testing laboratory for recognition in cracked and uncracked concrete including seismic and wind loading (Category 1 anchors)
- Evaluated and qualified by an accredited independent testing laboratory for reliability against brittle failure, e.g. hydrogen embrittlement.

#### **GUIDE SPECIFICATIONS**

CSI Divisions: 03 16 00 - Concrete Anchors, 05 05 19 - Post-Installed Concrete Anchors. Anchors shall be Concrete Hangermate+ as supplied by DEWALT, Towson, MD. Anchors shall be installed in accordance with published instruction and the Authority Having Jurisdiction.

#### **MATERIAL SPECIFICATIONS**

Anchor component	Specification				
Anchor Body	Case hardened low carbon steel				
Plating	Zinc plating according to ASTM B 633, SC1 Type III (Fe/Zn 5). Minimum plating requirements for Mild Service Condition.				

#### SECTION CONTENTS

General Information	1
Material Specifications	1
Installation Specifications	2
Installation Instructions	3
Reference Data (ASD)	4
Performance Data (SD)	6
Ordering Information	11



CONCRETE HANGERMATE+ (INTERNALLY THREADED COUPLER HEAD)



CONCRETE HANGERMATE+ (EXTERNAL THREAD - STUD HEAD)

#### THREAD VERSION

• Zinc Plated Carbon Steel

#### ANCHOR SIZE RANGE (TYP.)

• 1/4" and 3/8" diameter (Threaded Heads)

- · Sand-lightweight concrete
- Concrete over steel deck









• Unified Coarse Thread (UNC)

#### ANCHOR MATERIALS

#### SUITABLE BASE MATERIALS

- Normal-weight concrete

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# ECHANICAL ANCHORS

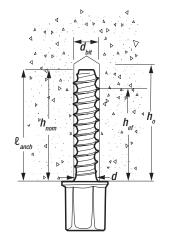
INSTALLATION	<b>SPECIFICATIONS</b>
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#### Installation Specifications for Hangermate+ in Concrete and Supplementary Information



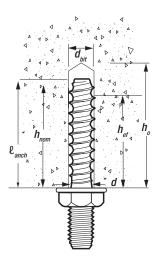
Anchor Property/	Notation	Units	Nominal Anchor Diameter (inch)					
	Setung mormation	Notation	Units	1/4				
Anchor outside diameter	Anchor outside diameter			0.250 (6.35)				
Nominal drill bit diameter		Clbit	in. (mm)	1/4 ANSI				
Minimum embedment dep	th	h <sub>nom</sub>	in. (mm)	1-5/8 2-1/2 (41) (64)				
Minimum hole depth		h₀	in. (mm)	2 2-7/8 (51) (73)				
Minimum member thickne	SS	h <sub>min</sub>	in. (mm)	3-1/4 4 (83) (102)				
Minimum edge distance		Cmin	in. (mm)	1-1/2 (38)				
Minimum spacing	Minimum spacing		in. (mm)	1-1/2 (38)				
Max. Installation torque	Max. Installation torque		ftlbf. (N-m)	19 (26)				
Max impact wrench power	(torque)	Timpact,max	ftlbf. (N-m)	150 (203)				
	Wrench socket size	1/4 thread 3/8 thread	in.	3/8 -				
Internal Threaded Head	Maximum head height	1/4 thread 3/8 thread	in.	33/64 - 43/64				
	Maximum washer diameter	1/4 thread	in.	1/2 -				
		3/8 thread		21/32				
Evtorpolly Throoded Llood	Wrench socket size Maximum head height	3/8 thread	in.	<u> </u>				
Externally Threaded Head Maximum head height Maximum washer diameter		3/6 tilleau	111.	21/32				
Effective tensile stress area (screw anchor body)		Ase	in.² (mm²)	0.045 (29.0)				
Minimum specified ultimate strength		f <sub>uta</sub>	ksi (N/mm²)	100 (690)				
Minimum specified yield st	rength	fy	ksi (N/mm²)	80 (552)				
For SI: 1 inch = 25.4 mm; 1 ks	i = 6.894 N/mm²; 1 ft-lb = 1.356 N	I-m; 1 lb = 0.004	4 kN.					

#### Hangermate+ Anchor Detail in Concrete



Internally Threaded

- $h_0 = Minimum Hole Depth$  $<math>\ell_{anch} = Nominal Anchor Length$



External Thread

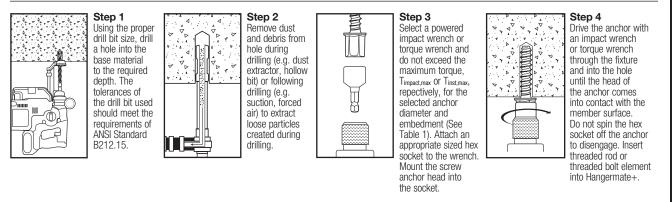


ECHANICAL ANCHORS

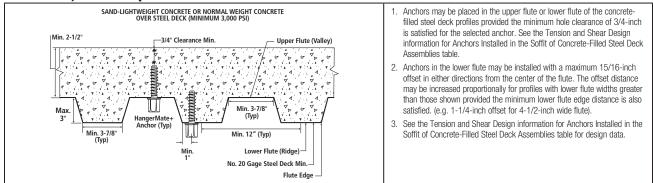
Rod Hanging Anchor

**CONCRETE HANGERI** 

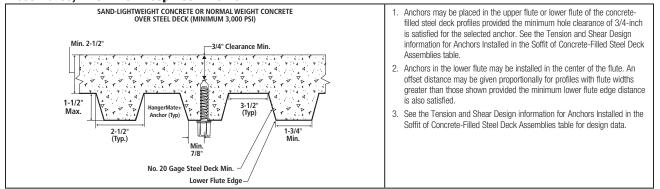
#### **INSTALLATION INSTRUCTIONS**



## Hangermate+ Installation Detail for Screw Anchors in the Soffit of Concrete over Steel Deck Floor and Roof Assemblies, 3-inch Deep Deck Profile<sup>1,2,3</sup>



## Hangermate+ Installation Detail for Screw Anchors in the Soffit of Concrete over Steel Deck Floor and Roof Assemblies, 1-1/2-inch Deep Deck Profile<sup>1,2,3</sup>



#### **REFERENCE DATA (ASD)**

#### Ultimate Load Capacities for Hangermate+ in Normal-Weight Concrete<sup>1,2</sup>

	Minimum	Minimum Concrete Compressive Strength										
Nominal Anchor	Nominal Embedment		500 psi MPa)	f <sup>i</sup> c = 3, (20.7	000 psi MPa)	f'c = 4, (27.6		f'c = 6, (41.4		f'c = 8, (55.2		
Diameter in.	Depth in. (mm)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	
1/4	1-5/8	2,835	1,485	2,995	1,525	3,265	1,525	3,265	1,525	3,265	1,525	
(1/4 Thread)	(41)	(12.6)	(6.6)	(13.3)	(6.8)	(14.5)	(6.8)	(14.5)	(6.8)	(14.5)	(6.8)	
1/4	1-5/8	2,835	2,035	2,995	2,090	3,265	2,090	3,265	2,090	3,265	2,090	
	(41)	(12.6)	(9.1)	(13.3)	(9.3)	(14.5)	(9.3)	(14.5)	(9.3)	(14.5)	(9.3)	
(3/8 Thread)	2-1/2	3,650	2,035	3,855	2,090	4,200	2,090	4,270	2,090	4,270	2,090	
	(64)	(16.2)	(9.1)	(17.1)	(9.3)	(18.7)	(9.3)	(19.0)	(9.3)	(19.0)	(9.3)	

1. Tabulated load values are for anchors installed in concrete. Concrete compressive strength must be at a minimum at the time of installation.

2. Ultimate load capacities must be reduced by a minimum safety factor of 4.0 or greater to determine allowable working load.

#### Allowable Load Capacities for Hangermate+ in Normal-Weight Concrete<sup>1,2,3,4</sup>



	Minimum	Minimum Concrete Compressive Strength										
Nominal Nominal		f'c = 2,500 psi		f'c = 3,000 psi		f'c = 4,000 psi		f'c = 6,000 psi		f'c = 8,000 psi		
Anchor Embedment		(17.3 MPa)		(20.7 MPa)		(27.6 MPa)		(41.4 MPa)		(55.2 MPa)		
Diameter in.	Depth in. (mm)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	Tension Ibs (kN)	Shear Ibs (kN)	
1/4	1-5/8	710	370	750	380	815	380	815	380	815	380	
(1/4 Thread)	(41)	(3.2)	(1.6)	(3.3)	(1.7)	(3.6)	(1.7)	(3.6)	(1.7)	(3.6)	(1.7)	
1/4	1-5/8	710	510	750	525	815	525	815	525	815	525	
	(41)	(3.2)	(2.3)	(3.3)	(2.3)	(3.6)	(2.3)	(3.6)	(2.3)	(3.6)	(2.3)	
(3/8 Thread)	2-1/2	915	510	965	525	1,050	525	1,070	525	1,070	525	
	(64)	(4.1)	(2.3)	(4.3)	(2.3)	(4.7)	(2.3)	(4.8)	(2.3)	(4.8)	(2.3)	

1. Tabulated load values are for anchors installed in concrete. Concrete compressive strength must be at the specified minimum at the time of installation.

2. Allowable load capacities are calculated using an applied safety factor 4.0.

3. Allowable load capacities must be multiplied by reduction factors when anchor spacing or edge distances are less than critical distances.

4. Linear interpolation may be used to determine allowable loads for intermediate embedments and compressive strengths.

**Edge Distance - Tension (F**<sub>NC</sub>)

#### Spacing - Tension (F<sub>NS</sub>)

Dia	ameter (in)		1/4	
Thre	ad Diameter	1/4"	3/8"	3/8"
Nominal Embedment, hnom (in) Minimum Edge Distance, Cmin (in)		1-5/8	1-5/8	2-1/2
		1-1/2	1-1/2	1-1/2
	1-1/2	0.77	0.77	0.64
-	1-3/4	0.83	0.83	0.67
ches	2	0.88	0.88	0.71
(ju	2-1/4	0.94	0.94	0.75
ance	2-1/2	1.00	1.00	0.78
Dist	2-3/4	1.00	1.00	0.82
Edge Distance (inches)	3	1.00	1.00	0.86
ũ	3-1/2	1.00	1.00	0.93
	4	1.00	1.00	1.00

- paoling								
Dia	ameter (in)		1/4					
Thre	ad Diameter	1-5/8	1-5/8	2-1/2				
Nominal E	mbedment, hnom (in)	1-1/5	1-1/5	2				
Minimum	Spacing, Smin (in)	3-3/5	3-3/5	5-5/6				
	1-1/2	0.77	0.77	0.68				
	1-3/4	0.80	0.80	0.70				
	2	0.83	0.83	0.72				
es)	2-1/4	0.86	0.86	0.74				
inch	2-1/2	0.89	0.89	0.76				
ce (j	2-3/4	0.92	0.92	0.78				
Spacing Distance (inches)	3	0.99	0.99	0.82				
g Di	3-1/2	1.00	1.00	0.86				
acin	4	1.00	1.00	0.90				
Spi	4-1/2	1.00	1.00	0.94				
	5	1.00	1.00	0.97				
	5-1/2	1.00	1.00	1.00				
	6	1.00	1.00	1.00				

#### **Edge Distance - Shear (Fvc)**

Dia	ameter (in)		1/4	
Thre	ad Diameter	1/4"	3/8"	3/8"
Nominal E	mbedment, hnom (in)	1-5/8	1-5/8	2-1/2
Minimum Ed	lge Distance, cmin (in)	1-1/2	1-1/2	1-1/2
	1-1/2	0.68	0.55	0.59
JCe	1-3/4	0.79	0.64	0.68
istaı hes)	2	0.90	0.73	0.78
Edge Distance (inches)	2-1/4	1.00	0.82	0.88
Edic	2-1/2	1.00	0.92	0.98
	2-3/4	1.00	1.00	1.00

#### Spacing - Shear (Fvs)

opuonig	phacing - Shear (FVS)								
Dia	ameter (in)		1/4						
Thre	ead Diameter	1/4"	3/8"	3/8"					
Nominal E	mbedment, hnom (in)	1-5/8	1-5/8	2-1/2					
Minimum	n Spacing, smin (in)	1-1/2	1-1/2	1-1/2					
	1-1/2	0.61	0.59	0.60					
	1-3/4	0.63	0.61	0.61					
	2	0.65	0.62	0.63					
	2-1/4	0.67	0.64	0.65					
	2-1/2	0.69	0.65	0.66					
~	2-3/4	0.71	0.67	0.68					
hes	3	0.73	0.68	0.70					
(inc	3-1/2	0.76	0.71	0.73					
ance	4	0.80	0.74	0.76					
Dista	4-1/2	0.84	0.77	0.79					
l gu	5	0.88	0.81	0.83					
Spacing Distance (inches)	5-1/2	0.91	0.84	0.86					
s	6	0.95	0.87	0.89					
	6-1/2	0.99	0.90	0.92					
	7	1.00	0.93	0.96					
	7-1/2	1.00	0.96	0.99					
	8	1.00	0.99	1.00					
	9	1.00	1.00	1.00					

ECHANICAL ANCHORS

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#### **PERFORMANCE DATA (SD)**

#### Hangermate+ Installation Specifications in Concrete and Supplemental Information<sup>1,2</sup>



					Martes Martes		
Anchor Pron	erty/Setting Information	Notation	Units	Nominal Anchor	Diameter (inch)		
Alichor Prop	erty/setung information	Notation	UIIIIS	1/	4		
Nominal anchor diameter		da	in. (mm)	0.2 (6.	4)		
Nominal drill bit diameter		d <sub>bit</sub>	in.	1/ AN	4 SI		
Minimum nominal embedme	nt depth <sup>3</sup>	h <sub>nom</sub>	in. (mm)	1-5/8 (41)	2-1/2 (64)		
Effective Embedment		h <sub>ef</sub>	in. (mm)	1.20 (30)	1.94 (49)		
Minimum hole depth		h₀	in. (mm)	2 (51)	2-7/8 (73)		
Minimum concrete member	thickness	h <sub>min</sub>	in. (mm)	3-1/4 (83)	4 (102)		
Minimum edge distance		Cmin	in. (mm)	1-1 (3			
Minimum spacing distance		Smin	in. (mm)	1-1 (3	/2 B)		
Critical edge distance		Cac	in. (mm)	4.30 (109)	6.10 (155)		
Minimum nominal anchor ler	ngth⁴	lanch	in. (mm)	1-5/8 (41)	2-1/2 (64)		
Max Installation torque		Tinst,max	ftlb. (N-m)	19 (26)	25 (34)		
Maximum impact wrench po	wer (torque)	Timpact,max	ftlb. (N-m)	150 (203)			
	Wrench socket size	1/4" thread 3/8" thread	- in.	3/8 -			
Internal Threaded Head	Maximum head height	1/4" thread 3/8" thread	- in.	33/64	-		
	Maximum washer diameter	1/4" thread 3/8" thread	in.	43/64 1/2 - 21/32			
	Wrench socket size	5/6 411040		1/			
Externally Threaded Head	Maximum head height	3/8" thread	in.	1-3,			
-	Maximum washer diameter	1		21/	32		
Effective tensile stress area (	screw anchor body)	A <sub>se</sub>	in² (mm²)	0.0 (29			
Minimum specified ultimate	strength	f <sub>uta</sub>	ksi (N/mm²)	10 (69			
Minimum specified yield stre	ngth	fy	ksi (N/mm²)	8 (55	2)		
Mean axial stiffness⁵	Uncracked concrete	$eta_{ ext{uncr}}$	lbf/in (kN/mm)	1,381 (24	-2)		
iviean axiai sunness"	Cracked concrete	$eta_{ m cr}$	lbf/in (kN/mm)	318, (5)			

For SI: 1 inch = 25.4 mm; 1 ksi =  $6.894 \text{ N/mm}^2$ ; 1 ft-lb = 1.356 N-m; 1 lb = 0.0044 kN.

1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable.

 For installations through the soffit of steel deck assemblies into concrete, see the design information table for installation in the soffit of concrete-filled steel deck assemblies and the installation details in the soffit of concrete over steel deck for the applicable steel deck profile. Tabulated minimum spacing values are based on anchors installed along the flute with axial spacing equal to the greater of 3her or 1.5 times the flute width.

3. The embedment depth, hnom, is measured from the outside surface of the concrete member to the embedded end of the anchor.

The listed minimum overall anchor length is based on the anchor sizes commercially available at the time of publication compared with the requirements to achieve the minimum nominal embedment depth, including consideration of a fixture attachment. The minimum nominal anchor length is measured from under the head to the tip of the anchor.
 Mean values shown, actual stiffness varies considerably depending on concrete strength, loading and geometry of application.

#### Tension Design Information for Hangermate+ Anchor is in Concrete<sup>1,2</sup>

DEWA

ENGINEERED BY POWERS



E <b>D</b> 39	A BLES

Nototion	11	Nominal Anchor Diameter		
Notation	Units	1/4	ļ	
1, 2 or 3	-	1		
h <sub>nom</sub>	in. (mm)	1-5/8 (41)	2-1/2 (64)	
eel Strength in Tension (ACI	318-14 17.4.1 or ACI 318-1	1 D.5.1)		
$N_{sa}^{10}$	lb (kN)			
$\phi$	-	0.6	5	
Breakout Strength in Tensi	on (ACI 318-14 17.4.2 or ACI	318-11 D.5.2)		
h <sub>ef</sub>	in. (mm)	1.20 (30)	1.94 (49)	
Cac	in. (mm)	4.30 (109)	6.10 (155)	
Kuncr	-	27	24	
k <sub>cr</sub>	-	17		
$\Psi_{c,N}$	-	1.0	)	
$\phi$	-	0.65 (Con	dition B)	
in Tension (Non-Seismic Ap	plications) (ACI 318-14 17.4.	3 or ACI 318-11 D.5.3)		
N <sub>p</sub> ,uncr	lb (kN)	See No	te 7	
N <sub>p,cr</sub>	lb (kN)	765 (3.4)	1,415 (6.3)	
$\phi$	-	0.65 (Con	dition B)	
n Tension for Seismic Appli	cations (ACI 318-14 17.2.3.3	Or ACI 318-11 D.3.3.3)		
N <sub>p,eq</sub>	lb (kN)	360 (1.6)	1,170 (5.2)	
$\phi$	-	0.65 (Con	dition B)	
	hnom eel Strength in Tension (ACI Nss <sup>10</sup>	1, 2 or 3         - $h_{nom}$ in. (mm)           cel Strength in Tension (ACI 318-14 17.4.1 or ACI 318-1 $N_{sa}^{10}$ Ib (kN) $\phi$ -           Breakout Strength in Tension (ACI 318-14 17.4.2 or ACI 318-14 17.4.2 or ACI 318-14 17.4.2 or ACI 16. $h_{ef}$ in. (mm)           Cac         (mm)           Cac         (mm)           Kunor         - $k_{cr}$ - $\psi_{CN}$ - $\psi_{CN}$ - $\psi_{CN}$ - $\phi$ -           in Tension (Non-Seismic Applications) (ACI 318-14 17.4. $N_{p,unor}$ Ib (kN) $\phi$ -           n Tension for Seismic Applications (ACI 318-14 17.2.3.3 $N_{p,eq}$ Ib (kN)	Notation         Units         Interaction           1, 2 or 3         -         1           hoom         in. (mm)         1-5/8 (41)         1           boom         10         1-5/8 (41)         1           eel Strength in Tension (ACI 318-14 17.4.1 or ACI 318-11 D.5.1)         1         1 $N_{a10}^{a10}$ lb         4,53 (kN)         (20.1 $\phi$ -         0.63           Breakout Strength in Tension (ACI 318-14 17.4.2 or ACI 318-11 D.5.2)         1           hef         in. (mm)         1.20 (30)         0 $C_{ac}$ in. (mm)         4.30 (109)         1           kuner         -         27         1 $K_{ar}$ -         1.0         0 $\phi$ -         0.65 (Conclean           in Tension (Non-Seismic Applications) (ACI 318-14 17.4.3 or ACI 318-11 D.5.3)         1 $N_{p,ar}$ lb         765 (kN)         1 $N_{p,ar}$ lb         765 (kN)         1 $\phi$ -         0.65 (Conclean         1 $n$ 10         360 (kN)         1         1	

For SI: 1 inch = 25.4 mm; 1 ksi = 6.894 N/mm<sup>2</sup>; 1 ft-lb = 1.356 N-m; 1 lb = 0.0044 kN.

1. The data in this table is intended to be used with the design provisions of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable; for anchors resisting seismic load combinations the additional requirements of ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable, shall apply.

2. Installation must comply with published instructions and details.

3. All values of  $\phi$  were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3, or ACI 318-11 Section 9.2. If the load combinations of ACI 318-11 Appendix C are used, then the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4. For reinforcement that complies with ACI 318-14 Chapter 17 or ACI 318-11 Appendix D requirements for Condition A, see ACI 318-14 17.3.3(c) or ACI 318-11 Section D.4.3(c), as applicable for the appropriate  $\phi$  factor when the load combinations of IBC Section 1605.2, ACI 318-11 Section D.4.3(c), as applicable for the appropriate  $\phi$  factor when the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used.

4. The anchors are considered a brittle steel elements as defined by ACI 318-14 2.3 or ACI 318-11 D.1, as applicable.

5. Select the appropriate effectiveness factor for cracked concrete (ker) or uncracked concrete (kuner) and use  $\Psi_{C,N} = 1.0$ .

6. For all design cases  $\Psi_{cP} = 1.0$ . The characteristic pullout strength, N<sub>PR</sub>, for concrete compressive strengths greater than 2,500 psi may be increased by multiplying the value in the table by (f'c / 2,500)<sup>a3</sup> for psi or (f'c / 17.2)<sup>a3</sup> for MPa.

7. Pullout strength does not control design of indicated anchors and does not need to be calculated for indicated anchor size and embedment.

8. Reported values for characteristic pullout strength in tension for seismic applications are based on test results per ACI 355.2, Section 9.5.

9. Anchors are permitted to be used in lightweight concrete provided the modification factor  $\lambda$ a equal to 0.8 $\lambda$  is applied to all values of  $\sqrt{1^{\circ}c}$  affecting Nn.

#### Shear Design Information for Hangermate+ Anchor in Concrete<sup>1,2,7,8</sup>



			Nominal Anchor Diameter				
Design Characteristic	Notation	Units					
Anchor category	1, 2 or 3	-	1		1		
Thread diameter	-	in.	1/4	3	/8		
Minimum nominal embedment depth	h <sub>nom</sub>	in. (mm)	1-5/8 (41)	1-5/8 (41)	2-1/2 (64)		
	Steel Strength i	in Shear (ACI 3	18-14 17.5.1 or ACI 318-11 D	).6.1)			
Steel strength in shear <sup>5</sup>	Vsa	lb (kN)	860 (3.8)	1,545 (6.9)	1,545 (6.9)		
Reduction factor for steel strength <sup>3,4</sup>	$\phi$	-	0.60				
Steel Stre	ngth in Shear for Se	ismic Applicat	ions (ACI 318-14 17.2.3.3 or )	ACI 318-11 D.3.3.3)			
Steel strength in shear, seismic6	Veq	lb (kN)	600 (2.7)	1,390 (6.2)	1,390 (6.2)		
Reduction factor for steel strength in shear for seismic <sup>3,4</sup>	φ	-		0.60			
Co	oncrete Breakout Str	ength in Shear	r (ACI 318-14 17.5.2 or ACI 31	8-11 D.6.2)			
Nominal anchor diameter	da	in. (mm)	0.250 (6.4)		250 4)		
Load bearing length of anchor	le	in. (mm)	1.20 (30)	1.20 1.94 (30) (49)			
Reduction factor for concrete breakout <sup>3</sup>	$\phi$	-	0.70 (Condition B)				
	Pryout Strength	in Shear (ACI :	318-14 17.5.3 or ACI 318-11	D.6.3)			
Coefficient for pryout strength	kcp	-	1	1	1		
Effective embedment	h <sub>ef</sub>	in. (mm)	1.20 (30)	1.20 1.94 (30) (49)			
Reduction factor for pryout strength <sup>3</sup>	φ	-		0.70 (Condition B)			

For SI: 1 inch = 25.4 mm; 1 ksi = 6.894 N/mm<sup>2</sup>; 1 ft-lb = 1.356 N-m; 1 lb = 0.0044 kN.

1. The data in this table is intended to be used with the design provisions of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable; for anchors resisting seismic load combinations the additional requirements of ACI 318-17 17.2.3 or ACI 318-11 D.3.3, as applicable shall apply.

2. Installation must comply with published instructions and details.

3. All values of  $\phi$  were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3, or ACI 318-11 Section 9.2. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 Section D.4.4. For reinforcement that complies with ACI 318-14 Chapter 17 or ACI 318-11 Appendix D requirements for Condition A, see ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c), as applicable, for the appropriate  $\phi$  factor when the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3, or ACI 318-11 Section 9.2 are used.

4. The anchors are considered a brittle steel elements as defined by ACI 318-14 2.3 or ACI 318-11 D.1.

5. Reported values for steel strength in shear are based on test results per ACI 355.2, Section 9.4 and must be used for design in lieu of the calculated results using equation 17.5.1.2(b) of ACI 318-14 or equation D-29 in ACI 318-11 D.6.1.2.

6. Reported values for steel strength in shear are for seismic applications and based on test results in accordance with ACI 355.2, Section 9.6 and must be used for design.

7. Anchors are permitted to be used in lightweight concrete in provided the modification factor  $\lambda$ a equal to 0.8 $\lambda$  is applied to all values of  $\sqrt{rc}$  affecting Nn.

Shear values are for threaded rod or steel inserts with an ultimate strength, F<sub>u</sub> ≥ 125 ksi; threaded rod or steel inserts with an F<sub>u</sub> less than 125 ksi are allowed provided the steel strength shear values are multiplied by the ratio of F<sub>u</sub> (ksi) of the steel insert and 125 ksi.



#### Tension and Shear Design Information for Hangermate+ Anchor in the Soffit (Through the Underside) of Concrete-Filled Steel Deck Assemblies<sup>1,2,3,4,5,6,7</sup>



1,960

(8.7)

0.60

(Infough the onderside) of concr		CI DOUR ASSO	1101103		
Anchor Property/Setting Information	Notation	Units		Nominal Anchor Size (inch)	
Anchor Category	1, 2 or 3	-	1		1
Head Style	-	-		Threaded	
Thread Diameter	-	in.	1/4	3	/8
Minimum nominal embedment depth	h <sub>nom</sub>	in. (mm)	1-5/8 (41)	1-5/8 (41)	2-1/2 (64)
Effective Embedment	h <sub>ef</sub>	in. (mm)	1.20 (30)	1.20 (30)	1.94 (49)
Minimum hole depth	h₀	in. (mm)	1-3/4 (44)	1-3/4 (44)	2-5/8 (67)
Anchors Installed Thro	ough the Soffit of St	eel Deck Assemblie	s into Concrete (Minimum 3	3-7/8-inch-wide deck flute)	
Minimum concrete member thickness <sup>a</sup>	h <sub>min,deck,total</sub>	in. (mm)	5-1/2 (140)		1/2 40)
Characteristic pullout strength, uncracked concrete over steel deck, (3,000 psi)	N <sub>p,deck,uncr</sub>	lb (kN)	1,430 (6.4)	1,430 (6.4)	2,555 (11.4)
Characteristic pullout strength, cracked concrete over steel deck, (3,000 psi)	N <sub>p,deck,cr</sub>	lb (kN)	615 (2.7)	615 (2.7)	1,115 (5.0)
Characteristic pullout strength, cracked concrete over steel deck, seismic, (3,000 psi)	N <sub>p,deck,eq</sub>	lb (kN)	290 (1.3)	290 (1.3)	920 (4.1)
Reduction factor for pullout strength <sup>9</sup>	φ	-		0.65	•
Steel strength in shear, concrete over steel deck	V <sub>sa,deck</sub>	lb (kN)	1,485 (6.6)		740 2.2)
Steel strength in shear, concrete over steel deck, seismic	Vsa,deck,eq	lb (kN)	1,040 (4.6)		465 1.0)
Reduction factor for steel strength in shear for concrete over steel deck <sup>a</sup>	φ	-		0.60	
Anchors Installed Thro	ough the Soffit of St	eel Deck Assemblie	s into Concrete (Minimum 1	-3/4-inch-wide deck flute)	
Minimum concrete member thickness <sup>8</sup>	h <sub>min,deck,total</sub>	in. (mm)	4 (102)		4 02)
Characteristic pullout strength, uncracked concrete over steel deck, (3,000 psi)	N <sub>p,deck,uncr</sub>	lb (kN)	1,760 (7.8)	1,760 (7.8)	2,075 (9.2)
Characteristic pullout strength, cracked concrete over steel deck, (3,000 psi)	N <sub>p,deck,cr</sub>	lb (kN)	760 (3.4)	770 (3.4)	910 (4.0)
Characteristic pullout strength, cracked concrete over steel deck,seismic, (3,000 psi)	N <sub>p,deck,eq</sub>	lb (kN)	355 (1.6)	635 (2.8)	750 (3.3)
Reduction factor for pullout strength <sup>8</sup>	$\phi$	-		0.65	-
Steel strength in shear, concrete over steel deck	Vsa,deck	lb (kN)	1,680 (7.5)		180 .7)

concrete over steel deck<sup>9</sup> For SI: 1 inch = 25.4 mm; 1 ksi = 6.894 N/mm<sup>2</sup>; 1 ft-lb = 1.356 N-m; 1 lb = 0.0044 kN.

1. Installation must comply with published instructions and details.

Steel strength in shear, concrete

Reduction factor for steel strength in shear for

over steel deck, seismic

2. Values for Np.deek.and Np.deek.ar are for sand-lightweight concrete (f'c, min = 3,000 psi) and additional lightweight concrete reduction factors need not be applied. In addition, evaluation for the concrete breakout capacity in accordance with ACI 318-14 17.4.2 or ACI 318 D.5.2, as applicable, is not required for anchors installed in the deck soffit (through underside).

1,175

(5.2)

lh

(kN)

3. Values for Np,deck,eq are applicable for seismic loading and must be used in lieu of Np,deck,cr.

4. For all design cases  $\Psi_{c,P} = 1.0$ . The characteristic pullout strength, Npn, for concrete compressive strengths greater than 3,000 psi anchors may be increased by multiplying the value in the table by (f'c / 3,000)03 for psi or (f'c / 17.2)03 for MPa.

5. Shear loads for anchors installed through steel deck into concrete may be applied in any direction.

6. Values of Vsadeck and Vsadeck are for sand-lightweight concrete and additional lightweight concrete reduction factors need not be applied. In addition, evaluation for the concrete breakout capacity in accordance with ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, and the pryout capacity in accordance with ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable, are not required for anchors installed in the soffit (through underside).

7. Shear values are for threaded rod or steel inserts with an ultimate strength, Fu ≥ 125 ksi; threaded rod or steel inserts with an Fu less than 125 ksi are allowed provided the steel strength shear values are multiplied by the ratio of  $\mathsf{F}_{u}$  (ksi) of the steel insert and 125 ksi.

8. The minimum concrete member thickness, hmin,deck,total, is the minimum overall thickness of the concrete-filled steel deck (depth and topping thickness).

Vsa,deck,eq

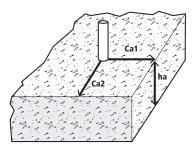
φ

9. All values of  $\phi$  were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318 Section 9.2. If the load combinations of ACI 318 Appendix C are used, then the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4 (ACI 318-08).



#### Factored Resistance Strength (ØNn And ØVn) Calculated In Accordance With ACI 318-14 Chapter 17:

- 1- Tabular values are provided for illustration and are applicable for single anchors installed in normal-weight
  - concrete with minimum slab thickness,  $h_a = h_{min}$ , and with the following conditions:  $c_{at}$  is greater than or equal to the critical edge distance,  $c_{ac}$  (table values based on  $c_{at} = c_{ac}$ ). -  $c_{a2}$  is greater than or equal to 1.5 times  $c_{a1}$ .
- 2- Calculations were performed according to ACI 318-14 Chapter 17. The load level corresponding to the controlling failure mode is listed. (e.g. For tension: steel, concrete breakout and pullout; For shear: steel, concrete breakout and pryout). Furthermore, the capacities for concrete breakout strength in tension and pryout strength in shear are calculated using the effective embedment values, hef, for the selected anchors as noted in the design information tables. Please also reference the installation specifications for more information.
- Strength reduction factors (ø) were based on ACI 318-14 Section 5.3 for load combinations. 3-Condition B is assumed.
- 4- Tabular values are permitted for static loads only, seismic loading is not considered with these tables.
- For designs that include combined tension and shear, the interaction of tension and shear loads must be 5calculated in accordance with ACI 318-14 Chapter 17.
- 6-Interpolation is not permitted to be used with the tabular values. For intermediate base material compressive strengths please see ACI 318-14 Chapter 17. For other design conditions including seismic considerations please see ACI 318-14 Chapter 17.





#### **Tension and Shear Design Strength Cracked Concrete**

	Nominal		Minimum Concrete Compressive Strength									
Nominal	Embed.	f'c = 2,	500 psi	f'c = 3,	000 psi	f'c = 4,	000 psi	f'C = 6,	000 psi	f'c = 8,	f'c = 8,000 psi	
Anchor Diameter	Depth hnom (in.)	øNn Tension (Ibs.)	øVn Shear (lbs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	
1/4" (1/4" thread)	1-5/8	495	515	525	515	575	515	645	515	705	515	
1/4"	1-5/8	495	780	525	855	575	925	645	925	705	925	
(3/8" thread)	2-1/2	920	925	970	925	1,060	925	1,195	925	1,305	925	

🔲 - Anchor Pullout/Pryout Strength Controls 🔲 - Concrete Breakout Strength Controls 🔲 - Steel Strength Controls

#### **Tension and Shear Design Strength Uncracked Concrete**



	Nominal		Minimum Concrete Compressive Strength								
Nominal	Embed.	f'c = 2,	f'c = 2,500 psi f'c = 3,000 psi		f'c = 4,	000 psi	f'c = 6,000 psi		f'c = 8,000 psi		
Anchor Diameter	Depth hnom (in.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)	øNn Tension (Ibs.)	øVn Shear (Ibs.)
1/4" (1/4" thread)	1-5/8	1,155	515	1,265	515	1,460	515	1,785	515	2,065	515
1/4"	1-5/8	1,155	925	1,265	925	1,460	925	1,785	925	2,065	925
(3/8" thread)	2-1/2	2,110	925	2,310	925	2,665	925	2,950	925	2,950	925
🗌 - Anchor Pullo	- Anchor Pullout/Pryout Strength Controls 🔲 - Concrete Breakout Strength Controls 🔲 - Steel Strength Controls										



#### **ORDERING INFORMATION**

							20V Max* S	20V Max* SDS Plus Rotary Hammers		
Catalog Number	Screw Size	Hang	Rod Size	Socket Size	Box Qty.	Ctn. Qty.	DCH273P2DH DCH133M2		DCH293R2 1-1/8" L-Shape w/ E-Clutch"	DCF883L2 3/8" Impact Wrench
								Carbide Bits		Impact Rated Socket
Hangermate	+ Internal	Thread		un fran fran fran fran						
PFM2211100	1/4" x 1-5/8"	Vertical	1/4"	3/8"	25	125	DW5517	DW5417	DW5417	DWMT19051B
PFM2211200	1/4" x 1-5/8"	Vertical	3/8"	1/2"	25	125	DW5517	DW5417	DW5417	DWMT19169B
PFM2211250	1/4" x 2-1/2"	Vertical	3/8"	1/2"	25	125	DW5517	DW5417	DW5417	DWMT19169B
Hangermate+ External Thread										
PFM1421000	1/4" x 1-5/8"	Vertical	3/8"	1/2"	25	125	DW5517	DW5417	DW5417	DWMT19052B
PFM1421050	1/4" x 2-1/2"	Vertical	3/8"	1/2"	25	125	DW5517	DW5417	DW5417	DWMT19052B
The published size	includes the diame	ter and length of t	he anchor measur	ed from under the	head.		<ul> <li>Optimum Tool</li> <li>Maximum Tool</li> </ul>			

#### **Zinc Economy Rod Coupling Nuts**

Catalog Number	Coupler Size	Box Qty.	Ctn. Qty.
030007	3/8" - 16 x 1/2" x 1-1/8"	100	1000

#### Zinc Reducing Rod Coupling Nuts

Catalog Number	Coupler Size	Box Qty.	Ctn. Qty.
030016	3/8"-16 - 1/4"-20	50	1000
030017	1/2"-13 - 3/8"-16	50	500





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## **ESR-3889**

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DIVISION: 03 00 00—CONCRETE SECTION: 03 16 00—CONCRETE ANCHORS DIVISION: 05 00 00—METALS SECTION: 05 05 19—POST-INSTALLED CONCRETE ANCHORS

**REPORT HOLDER:** 

DEWALT

**EVALUATION SUBJECT:** 

SCREW-BOLT+<sup>™</sup> SCREW ANCHORS AND HANGERMATE<sup>®</sup>+ ROD HANGER SCREW ANCHORS IN CRACKED AND UNCRACKED CONCRETE (DEWALT)



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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00—METALS Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

DEWALT

ADDITIONAL LISTEE:

#### THE HILLMAN GROUP

#### **EVALUATION SUBJECT:**

SCREW-BOLT+™ SCREW ANCHORS AND HANGERMATE<sup>®</sup>+ ROD HANGER SCREW ANCHORS IN CRACKED AND UNCRACKED CONCRETE (DEWALT)

#### **1.0 EVALUATION SCOPE**

Compliance with the following codes:

- 2018, 2015, 2012 and 2009 *International Building Code*<sup>®</sup> (IBC)
- 2018, 2015, 2012 and 2009 International Residential Code<sup>®</sup> (IRC)

For evaluation for compliance with codes adopted by Los Angeles Department of Building and Safety (LADBS), see ESR-3889 LABC and LARC Supplement.

#### Property evaluated:

Structural

#### 2.0 USES

The Screw-Bolt+ screw anchors and Hangermate+ rod hanger screw anchors are used as anchorage in cracked and uncracked normal-weight concrete and lightweight concrete having a specified compressive strength,  $f'_c$ , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa) to resist static, wind and seismic tension and shear loads.

The  ${}^{1}/_{4}$ -inch-,  ${}^{3}/_{8}$ -inch- and  ${}^{1}/_{2}$ -inch-diameter (6.4 mm, 9.5 mm and 12.7 mm) Screw-Bolt+ anchors may be installed in the topside of cracked and uncracked normal-weight or sand-lightweight concrete-filled steel deck having a specified compressive strength,  $f'_{c}$ , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

The  ${}^{1}$ /<sub>4</sub>-inch-,  ${}^{3}$ /<sub>8</sub>-inch-,  ${}^{1}$ /<sub>2</sub>-inch-,  ${}^{5}$ /<sub>8</sub>-inch, and  ${}^{3}$ /<sub>4</sub>-inchdiameter (6.4 mm 9.5 mm, 12.7 mm, 15.9 mm and A Subsidiary of the International Code Council®

19.1 mm) Screw-Bolt+ anchors may be installed in the soffit of cracked and uncracked normal-weight or sand-lightweight concrete-filled steel deck having a minimum specified compressive strength,  $f'_c$ , of 3,000 psi (20.7 MPa).

The  ${}^{1}/_{4}$ -inch- and  ${}^{3}/_{8}$ -inch-diameter (6.4 mm and 9.5 mm) Hangermate+ anchors may be installed in the soffit of cracked and uncracked normal-weight or sand-lightweight concrete-filled steel deck having a minimum specified compressive strength,  $f'_{c}$ , of 3,000 psi (20.7 MPa).

The anchors are an alternative to cast-in-place anchors described in Section 1901.3 of the 2018 and 2015 IBC, Section 1908 and 1909 of the 2012 IBC, and Sections 1911 and 1912 of the 2009 IBC. The anchors may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the IRC.

#### 3.0 DESCRIPTION

#### 3.1 Screw-Bolt+ Anchors:

Screw-Bolt+ screw anchors are comprised of an anchor body with hex washer head. Available diameters are  $1_{4}$ -inch,  $3_{8}$ -inch,  $1_{2}$ -inch,  $5_{8}$ -inch and  $3_{4}$ -inch (6.4 mm, 9.5 mm, 12.7 mm, 15.9 mm and 19.1 mm). The anchor body and hex washer head are manufactured from low-carbon steel which is case hardened and have minimum 0.0002-inch (5 µm) zinc plating in accordance with ASTM B633 or minimum 0.0021-inch (53 µm) mechanical zinc plating in accordance with ASTM B695, Class 55. The Screw-Bolt+ screw anchor is illustrated in Figures 1A and 1B. Product names for the report holder and for the additional listees are presented in the following table.

COMPANY NAME	PRODUCT NAME
DEWALT	Screw-Bolt+
The Hillman Group	Hillman Screw-Bolt+

The hex head of the anchor is formed with an integral washer and serrations on the underside. The anchor body is formed with dual lead threads and a chamfered tip. The screw anchors are installed in a predrilled hole with a powered impact wrench or torque wrench. The threads on the anchor tap into the sides of the predrilled hole and interlock with the base material during installation.

#### 3.2 Hangermate+ Anchors:

Hangermate+ rod hanger screw anchors are comprised

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of a nominally  $^{1}/_{4}$ -inch-diameter one-piece anchor body, with a hex coupler head version containing internal threads that accepts threaded rods and bolts in  $^{1}/_{4}$ -inch and  $^{3}/_{8}$ -inch (6.4 mm and 9.5 mm) diameters or a stud head version containing external threads in  $^{3}/_{8}$ -inch (9.5 mm) diameter.

The anchor body and hex coupler head are manufactured from low-carbon steel which is case hardened, and have minimum 0.0002-inch (5  $\mu$ m) zinc plating in accordance with ASTM B633. The Hangermate+ rod hanger screw anchor is illustrated in Figures 1A and 1B.

Product names for the report holder and for the additional listees are presented in the following table.

COMPANY NAME	PRODUCT NAME
DEWALT	Hangermate+
The Hillman Group	Hillman Hangermate+

The hex coupler head of the anchor is formed with serrations on the underside, and with internal threads into the topside that accepts threaded rods or threaded bolt steel insert elements. The anchor body is formed with dual lead threads and a chamfered tip. The anchors are installed in a predrilled hole with a powered impact wrench or torque wrench. The threads on the anchor body tap into the sides of the predrilled concrete hole and interlock with the base material during installation.

## 3.3 Threaded Steel Insert Elements for Hangermate+:

Threaded steel insert elements must be threaded into the Hangermate+ anchors to form a connection. The material properties of the steel inserts must comply national or international specifications (e.g., ASTM A36; ASTM A307, ASTM F1554, Grade 36; ASTM A307, SAE J429, Grade 2, ASTM A193, Grade B7), or equivalent.

#### 3.4 Concrete:

Normal-weight and lightweight concrete must conform to Sections 1903 and 1905 of the IBC.

#### 3.5 Steel Deck Panels:

Steel deck panels for anchors must comply with the configurations in Figures 5A, 5B, 6A and 6B of this report, and have a minimum base-metal thickness of 0.035 inch (0.89 mm) [No. 20 gage]. Steel deck must comply with ASTM A653/A 653M SS Grade 50, and have a minimum yield strength of 50 ksi (345 MPa).

#### 4.0 DESIGN AND INSTALLATION

#### 4.1 Strength Design:

**4.1.1 General:** Design strength of anchors complying with the 2018 and 2015 IBC, as well as Section R301.1.3 of the 2018 and 2015 IRC must be determined in accordance with ACI 318-14 Chapter 17 and this report.

Design strength of anchors complying with the 2012 IBC, as well as Section R301.1.3 of the 2012 IRC, must be determined in accordance with ACI 318-11 Appendix D and this report.

Design strength of anchors complying with the 2009 IBC, as well as Section R301.1.3 of the 2009 IRC, must be determined in accordance with ACI 318-08 Appendix D and this report.

A design example in accordance with the 2018, 2015 and 2012 IBC is given in Figure 7 of this report.

Design parameters provided in Tables 3, 4 and 5 of this report are based on the 2018 and 2015 IBC (ACI 318-14) and the 2012 IBC (ACI 318-11) unless noted otherwise in Section 4.1.1 through 4.1.12 of this report.

The strength design of anchors must comply with ACI 318-14 17.3.1 or ACI 318-11 D.4.1, as applicable, except as required in ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable. Strength reduction factors,  $\phi$ , as given in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, and noted in Tables 3, 4 and 5 of this report, must be used for load combinations calculated in accordance with Section 1605.2 of the IBC, Section 5.3 of ACI 318-14, and Section 9.2 of ACI 318-11, as applicable. Strength reduction factors,  $\phi$ , as given in ACI 318-11 D.4.4 must be used for load combinations calculated in accordance with Appendix C of ACI 318-11. The value of  $f'_c$  used in the calculation must be limited to a maximum of 8,000 psi (55.2 MPa), in accordance with ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable.

**4.1.2 Requirements for Static Steel Strength in Tension**,  $N_{sa}$ : The nominal static steel strength of a single anchor in tension,  $N_{sa}$ , calculated in accordance with ACI 318-14 17.4.1.2 or ACI 318-11 D.5.1.2, as applicable, is given in Table 3 of this report. Strength reduction factors,  $\phi$ , corresponding to brittle steel elements must be used.

4.1.3 Requirements for Static Concrete Breakout Strength in Tension, N<sub>cb</sub> or N<sub>cbg</sub>: The nominal concrete breakout strength of a single anchor or a group of anchors in tension,  $N_{cb}$  or  $N_{cbg}$ , respectively, must be calculated in accordance with ACI 318-14 17.4.2 or ACI 318-11 D.5.2, as applicable, with modifications as described in this section. The basic concrete breakout strength of a single anchor in tension in cracked concrete, N<sub>b</sub>, must be calculated according to ACI 318-14 17.4.2.2 or ACI 318-11 D.5.2.2, as applicable, using the values of  $h_{ef}$  and  $k_{cr}$  as given in Table 3 of this report. The nominal concrete breakout strength in tension in regions where analysis indicates no cracking in accordance with ACI 318-14 17.4.2.6 or ACI 318-11 D.5.2.6, as applicable, must be calculated with the value of  $k_{uncr}$  as given in Table 3 of this report and with  $\psi_{c,N} = 1.0$ .

For anchors installed in the soffit of sand-lightweight or normal-weight concrete filled steel deck floor and roof assemblies, as shown in Figures 5A, 5B, 6A and 6B, calculation of the concrete breakout strength in accordance with ACI 318-14 17.4.2 or ACI 318-11 D.5.2, as applicable, is not required.

**4.1.4 Requirements for Static Pullout Strength in Tension**, *N*<sub>pn</sub>: The nominal pullout strength of a single anchor or a group of anchors, in accordance with ACI 318-14 17.4.3 or ACI 318-11 D.5.3, as applicable, in cracked and uncracked concrete, *N*<sub>p,cr</sub> and *N*<sub>p,uncr</sub>, respectively, is given in Table 3. In lieu of ACI 318-14 17.4.3.6 or ACI 318-11 D.5.3.6, as applicable,  $\Psi_{c,P} = 1.0$ for all design cases. The nominal pullout strength in cracked concrete may be adjusted by calculation according to Eq-1:

$$N_{pn,f_c'} = N_{p,cr} \left(\frac{f_c'}{2,500}\right)^n$$
 (lb, psi) (Eq-1)  
 $N_{pn,f_c'} = N_{p,cr} \left(\frac{f_c'}{17.2}\right)^n$  (N, MPa)

where  $f'_c$  is the specified concrete compressive strength and *n* is the factor defining the influence of concrete compressive strength on pullout strength. For the

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 $1/_4$ -inch-diameter anchors, *n* is 0.3. For all other cases, *n* is 0.5.

In regions where analysis indicates no cracking in accordance with ACI 318-14 17.4.3.6 or ACI 318-11 D.5.3.6, as applicable, the nominal pullout strength in tension of the anchors can be adjusted by calculation according to Eq-2:

$$N_{pn,f_c'} = N_{p,uncr} \left(\frac{f_c'}{2,500}\right)^n \text{ (lb, psi)}$$
(Eq-2)  
$$N_{pn,f_c'} = N_{p,uncr} \left(\frac{f_c'}{17.2}\right)^n \text{ (N,MPa)}$$

where  $f'_c$  is the specified concrete compressive strength and *n* is the factor defining the influence of concrete compressive strength on pullout strength. For the  $1/_4$ -inch-diameter anchors, *n* is 0.3. For all other cases, *n* is 0.5.

Where values for  $N_{p,cr}$  or  $N_{p,uncr}$  are not provided in Table 3 of this report, the pullout strength in tension need not be considered or evaluated.

The nominal pullout strength in tension of anchors installed in the upper and lower flute soffit of sand-lightweight or normal-weight concrete-filled steel deck floor and roof assemblies, as shown in Figures 5A, 5B, 6A and 6B, is provided in Table 5. The nominal pullout strength in cracked concrete can be adjusted by calculation according to Eq-1, whereby the value of  $N_{p,deck,cr}$  must be substituted for  $N_{p,cr}$  and the value of 3,000 psi (20.7 MPa) must be substituted for the value of 2,500 psi (17.2 MPa) in the denominator. The nominal pullout strength in uncracked concrete can be adjusted by calculation according to Eq-2, whereby the value of  $N_{p,deck,uncr}$  must be substituted for  $N_{p,uncr}$  and the value of 3,000 psi (20.7 MPa) must be substituted for the value of 2,500 psi (17.2 MPa) must be substituted for the value of  $N_{p,deck,uncr}$  must be substituted for  $N_{p,uncr}$  and the value of 3,000 psi (20.7 MPa) must be substituted for the value of 2,500 psi (17.2 MPa) in the denominator.

**4.1.5 Requirements for Static Steel Strength in Shear,**  $V_{sa}$ : The nominal steel strength in shear,  $V_{sa}$ , of a single anchor in accordance with ACI 318-14 17.5.1.2 or ACI 318-11 D.6.1.2, as applicable, is given in Table 4 of this report and must be used in lieu of the values derived by calculation from ACI 318-14 Eq, 17.5.1.2b or ACI 318-11, Eq. D-29, as applicable. Strength reduction factors,  $\phi$ , corresponding to brittle steel elements must be used.

The nominal shear strength of anchors installed in the soffit of sand-lightweight or normal-weight concrete-filled steel deck floor and roof assemblies,  $V_{sa,deck}$ , as shown in Figures 5A, 5B, 6A and 6B is given in Table 5 of this report, in lieu of the values derived by calculation from ACI 318-14 Eq. 17.5.1.2b or ACI 318-11, Eq. D-29, as applicable.

**4.1.6 Requirements for Static Concrete Breakout Strength in Shear,**  $V_{cb}$  **or**  $V_{cbg}$ **:** The nominal concrete breakout strength of a single anchor or group of anchors in shear,  $V_{cb}$  or  $V_{cbg}$ , respectively, must be calculated in accordance with ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, with modifications as described in this section. The basic concrete breakout strength of a single anchor in shear,  $V_b$ , must be calculated in accordance with ACI 318-14 17.5.2.2 or ACI 318-11 D.6.2.2, as applicable, using the value of  $\ell_e$ and  $d_a$  given in Table 4 of this report.

For anchors installed in the topside of concrete-filled steel deck assemblies, the nominal concrete breakout strength of a single anchor or group of anchors in shear,  $V_{cb}$  or  $V_{cbg}$ , respectively, must be calculated in accordance with ACI 318-14 17.5.2 or ACI 318-11

D.6.2, as applicable, using the actual member topping thickness,  $h_{min,deck}$ , in the determination of  $A_{vc}$ . Minimum member topping thickness for anchors in the topside of concrete-filled steel deck assemblies is given in Tables 1 and 2 of this report, as applicable.

For anchors installed in the soffit of sand-lightweight or normal-weight concrete filled steel deck floor and roof assemblies, as shown in Figures 5A, 5B, 6A and 6B, calculation of the concrete breakout strength in accordance with ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, is not required.

**4.1.7 Requirements for Static Concrete Pryout Strength in Shear**,  $V_{cp}$  or  $V_{cpg}$ : The nominal concrete pryout strength of a single anchor or group of anchors,  $V_{cp}$  or  $V_{cpg}$ , respectively, must be calculated in accordance with ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable, using the value of  $k_{cp}$  provided in Table 4, and the value of  $N_{cb}$  or  $N_{cbg}$  as calculated in Section 4.1.3 of this report.

For anchors installed in the soffit of sand-lightweight or normal-weight concrete filled steel deck floor and roof assemblies, as shown in Figures 5A, 5B, 6A and 6B, calculation of the concrete pryout strength in accordance with ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable, is not required.

#### 4.1.8 Requirements for Seismic Design:

**4.1.8.1 General:** For load combinations including seismic loads, the design must be performed in accordance with ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable. Modifications to ACI 318-14 17.2.3 shall be applied under 2018 and 2015 IBC Section 1905.1.8. For the 2012 IBC, Section 1905.1.9 shall be omitted. Modifications to ACI 318-08 D.3.3 shall be applied under Section 1908.1.9 of the 2009 IBC.

The nominal steel strength and nominal concrete breakout strength for anchors in tension, and the nominal concrete breakout strength and pryout strength for anchors in shear, must be calculated according to ACI 318-14 17.4 and 17.5 or ACI 318-11 D.5 and D.6, respectively, as applicable, taking into account the corresponding values in Tables 3 and 4 of this report.

The anchors comply with ACI 318-14 2.3 or ACI 318-11 D.1, as applicable, as brittle steel elements and must be designed in accordance with ACI 318-14 17.2.3.4, 17.2.3.5, 17.2.3.6, or 17.2.3.7; ACI 318-11 D.3.3.4, D.3.3.5, D.3.3.6 or D.3.3.7; or ACI 318-08 D.3.3.4, D.3.3.5 or D.3.3.6, as applicable.

The  ${}^{1}/_{4}$ -inch-diameter (6.4 mm),  ${}^{3}/_{8}$ -inch-diameter (9.5 mm),  ${}^{1}/_{2}$ -inch-diameter (12.7 mm),  ${}^{5}/_{8}$ -inch-diameter (15.9 mm) and  ${}^{3}/_{4}$ -inch-diameter (19.1 mm) Screw-Bolt+ anchors and the  ${}^{1}/_{4}$ -inch-diameter (6.4 mm) and  ${}^{3}/_{8}$ -inch-diameter (9.5 mm) Hangermate+ anchors may be installed in regions designated as IBC Seismic Design Categories A through F.

**4.1.8.2 Seismic Tension:** The nominal steel strength and nominal concrete breakout strength for anchors in tension must be calculated according to ACI 318-14 17.4.1 and 17.4.2, or ACI 318-11 D.5.1 and D.5.2, respectively, as applicable, as described in Sections 4.1.2 and 4.1.3 of this report. In accordance with ACI 318-14 17.4.3.2 or ACI 318-11 D.5.3.2, as applicable, the appropriate value for nominal pullout strength in tension for seismic loads,  $N_{p,eq}$  described in Table 3 of this report, must be used in lieu of  $N_p$ .  $N_{p,eq}$  may be adjusted by calculations for concrete compressive strength in accordance with Eq-1 of this report.

Where values for  $N_{p,eq}$  are not provided in Table 3, the pullout strength in tension for seismic forces need not be evaluated.

For anchors installed in the soffit of sand-lightweight or normal-weight concrete-filled steel deck floor and roof assemblies, the nominal pullout strength in tension for seismic loads,  $N_{p,deck,eq}$ , is provided in Table 5 and must be used in lieu of  $N_{p,cr}$ .  $N_{p,deck,eq}$  may be adjusted by calculations for concrete compressive strength in accordance with Eq-1 of this report where the value of 3,000 psi or 20.7 MPa must be substituted for the value of 2,500 psi or 17.2 MPa in the denominator.

**4.1.8.3 Seismic Shear:** The nominal concrete breakout strength and pryout strength for anchors in shear must be calculated according to ACI 318-14 17.5.2 or 17.5.3, or ACI 318-11 D.6.2 and D.6.3, respectively, as applicable, as described in Sections 4.1.6 and 4.1.7 of this report. In accordance with ACI 318-14 17.5.1.2 or ACI 318-11 D.6.1.2, as applicable, the appropriate value for nominal steel strength in shear for seismic loads,  $V_{sa,eq}$ , described in Table 4 of this report, must be used in lieu of  $V_{sa}$ .

For anchors installed in the soffit of sand-lightweight or normal-weight concrete-filled steel deck floor and roof assemblies, as shown in Figures 5A, 5B, 6A and 6B, the appropriate value for nominal steel strength in shear for seismic loads,  $V_{sa.deck,eq}$ , described in Table 5, must be used in lieu of  $V_{sa}$ .

**4.1.9 Requirements for Interaction of Tensile and Shear Forces:** The effects of combined tensile and shear forces must be determined in accordance with ACI 318-14 17.6 or ACI 318-11 D.7, as applicable.

**4.1.10 Requirements for Critical Edge Distance**,  $c_{ac}$ : In applications where  $c < c_{ac}$  and supplemental reinforcement to control splitting of the concrete is not present, the concrete breakout strength in tension for uncracked concrete, calculated according to ACI 318-14 17.4.2 or ACI 318-11 D.5.2, as applicable, must be further multiplied by the factor  $\psi_{cp,N}$  given by Eq-3:

$$\psi_{cp,N} = \frac{c}{c_{cr}}$$
(Eq-3)

whereby the factor  $\psi_{cp,N}$  need not be taken less than  $\frac{1.5h_{ef}}{c_{ac}}$ . For all other cases,  $\psi_{cp,N} = 1.0$ . In lieu of using ACI 318-14 17.7.6 or ACI 318-11 D.8.6, as applicable, values of  $c_{ac}$  provided in Tables 1 and 2 of this report must be used.

**4.1.11 Requirements for Minimum Member Thickness, Minimum Anchor Spacing and Minimum Edge Distance:** In lieu of ACI 318-14 17.7.1 and 17.7.3, or ACI 318-11 D.8.1 and D.8.3, respectively, as applicable, the values of  $s_{min}$  and  $c_{min}$  as given in Table 1 of this report must be used. In lieu of ACI 318-14 17.7.5 or ACI 318-11 D.8.5, as applicable, minimum member thicknesses,  $h_{min}$ , as given in Table 1 of this report must be used.

For anchors installed in the topside of concrete-filled steel deck assemblies, the anchors must be installed in accordance with Tables 1 and 2 and Figure 4 of this report.

For anchors installed through the soffit of steel deck assemblies, the anchors must be installed in accordance with Figures 5A, 5B, 6A, and 6B, and shall have an axial spacing along the flute equal to the greater of  $3h_{ef}$  or 1.5 times the flute width.

**4.1.12 Requirements for Lightweight Concrete:** For the use of anchors in lightweight concrete, the modification factor  $\lambda_a$  equal to  $0.8\lambda$  is applied to all values of  $\sqrt{f_c}$  affecting  $N_n$  and  $V_n$ .

For ACI 318-14 (2018 and 2015 IBC), ACI 318-11 (2012 IBC) and ACI 318-08 (2009 IBC),  $\lambda$  shall be determined in accordance with the corresponding version of ACI 318.

For anchors installed in the soffit of sand-lightweight concrete-filled steel deck and floor and roof assemblies, further reduction of the pullout values provided in this report is not required.

#### 4.2 Allowable Stress Design (ASD):

**4.2.1 General:** Design values for use with allowable stress design load combinations calculated in accordance with Section 1605.3 of the IBC must be established using Eq-4 and Eq-5 as follows:

$$T_{allowable,ASD} = \frac{\phi N_n}{\alpha}$$
 (Eq-4)

$$V_{allowable,ASD} = \frac{\phi V_n}{\alpha}$$
 (Eq-5)

where:

T <sub>allowable,ASD</sub>	=	Allowable tension load (lbf or kN)	
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- $V_{allowable,ASD}$  = Allowable shear load (lbf or kN)
- $\phi N_n$  = Lowest design strength of an anchor or anchor group in tension as determined in accordance with ACI 318-14 Chapter 17 and 2018 and 2015 IBC Section 1905.1.8, ACI 318-11 Appendix D, ACI 318-08 Appendix D and 2009 IBC Section 1908.1.9, and Section 4.1 of this report, as applicable (lbf or kN).
- $\phi V_n$  = Lowest design strength of an anchor or anchor group in shear as determined in accordance with ACI 318-14 Chapter 17 and 2018 and 2015 IBC Section 1905.1.8, ACI 318-11 Appendix D, ACI 318-08 Appendix D and 2009 IBC Section 1908.1.9, and Section 4.1 of this report, as applicable (Ibf or kN).
- $\alpha$  = Conversion factor calculated as a weighted average of the load factors for the controlling load combination. In addition,  $\alpha$  must include all applicable factors to account for non-ductile failure modes and required over-strength.

The limits on edge distance, anchor spacing and member thickness as given in Tables 1 and 2 of this report must apply. An example of Allowable Stress Design tension values for illustrative purposes is shown in Table 6 of this report.

**4.2.2 Interaction of Tensile and Shear Forces:** The interaction must be calculated and consistent with ACI 318-14 17.6 or ACI 318 (-11, -08) D.7, as applicable, as follows:

For shear loads  $V \le 0.2 V_{allowable,ASD}$ , the full allowable load in tension  $T_{allowable,ASD}$  must be permitted.

For tension loads  $T \le 0.2 T_{allowable,ASD}$ , the full allowable load in shear  $V_{allowable,ASD}$  must be permitted.

For all other cases: 
$$\frac{T}{T_{allowable}} + \frac{V}{V_{allowable}} \le 1.2$$
 (Eq-6)

#### 4.3 Installation:

Installation parameters are provided in Tables 1 and 2, and Figures 1A, 2 and 3 of this report. Anchor locations must comply with this report and plans and specifications approved by the code official. The Screw-Bolt+ and Hangermate+ screw anchors must be installed according to the manufacturer's published installation instructions and this report. Recommendations for installation equipment are given in Table A. Anchors must be installed in holes drilled using carbide-tipped masonry drill bits complying with ANSI B212.15.

The Screw-Bolt+ and Hangermate+ screw anchors are permitted to be loosened by a maximum of one full turn and retightened with a torque wrench or powered impact wrench to facilitate fixture attachment or realignment. Complete removal and reinstallation of the anchor is not allowed.

For anchor installation in the topside of concrete-filled steel deck assemblies, installation must comply with Tables 1 and 2 and Figure 4, as applicable.

For installation in the soffit of concrete on steel deck assemblies, the hole diameter in the steel deck must not exceed the diameter of the hole in the concrete by more than  $^{1}/_{8}$  inch (3.2 mm). For member thickness and edge distance restrictions for installations into the soffit of concrete on steel deck assemblies, see Table 5 and Figures 5A, 5B, 6A, and 6B.

#### 4.4 Special Inspection:

Periodic special inspection is required, in accordance with Section 1705.1.1 and Table 1705.3 of the 2018 and 2015 IBC or 2012 IBC, as applicable; Section 1704.15 and Table 1704.4 of the 2009 IBC; or Section 1704.13 of the 2006 IBC, as applicable. The special inspector must make periodic inspections during anchor installation to verify anchor type, anchor dimensions, concrete type, concrete compressive strength, hole dimensions, drill bit size and type, anchor spacing, edge distances, concrete thickness, anchor embedment, maximum impact wrench power and adherence to the manufacturer's published installation instructions. The special inspector must be present as often as required in accordance with the "statement of special inspection."

#### 5.0 CONDITIONS OF USE

The Screw-Bolt+ and Hangermate+ screw anchors described in this report comply with, or are a suitable alternative to what is specified in, those codes listed in Section 1.0 of this report, subject to the following conditions:

- **5.1** The anchors must be installed in accordance with the manufacturer's published installation instructions and this report. In case of a conflict, this report governs.
- **5.2** Anchor sizes, dimensions, and minimum embedment depths are as set forth in this report.
- **5.3** The  $^{1}/_{4}$ -inch to  $^{3}/_{4}$ -inch (6.4 mm to 19.1 mm) Screw-Bolt+ anchors and  $^{1}/_{4}$ -inch- and  $^{3}/_{8}$ -inchdiameter (6.4 mm and 9.5 mm) Hangermate+ anchors must be installed in cracked and uncracked normal-weight concrete and lightweight concrete having a specified compressive strength,  $f'_{c}$ , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).
- **5.4** The <sup>1</sup>/<sub>4</sub>-inch to <sup>1</sup>/<sub>2</sub>-inch (6.4 mm to 12.7 mm) Screw-Bolt+ anchors may be installed in the topside of cracked and uncracked normal-weight or

sand-lightweight concrete-filled steel deck having a minimum specified compressive strength,  $f'_{c}$ , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

- **5.5** The  ${}^{1}/_{4}$ -inch to  ${}^{3}/_{4}$ -inch (6.4 mm to 19.1 mm) Screw-Bolt+ anchors and  ${}^{1}/_{4}$ -inch- and  ${}^{3}/_{8}$ -inch-inchdiameter (6.4 mm and 9.5 mm) Hangermate+ anchors must be installed in the soffit of cracked and uncracked normal-weight or sand-lightweight concrete-filled steel deck having a minimum specified compressive strength,  $f'_{c_{7}}$  of 3,000 psi (20.7 MPa).
- **5.6** The values of  $f'_c$  used for calculation purposes must not exceed 8,000 psi (55.2 MPa).
- **5.7** The concrete shall have attained its minimum design strength prior to installation of the anchors.
- **5.8** Strength design values must be established in accordance with Section 4.1 of this report.
- **5.9** Allowable design values must be established in accordance with Section 4.2 of this report.
- **5.10** Anchor spacing(s) and edge distance(s), and minimum member thickness, must comply with Tables 1 and 2, and Figures 4, 5A, 5B, 6A, and 6B of this report.
- **5.11** Reported values for the Hangermate+ with an internally threaded head do not consider the steel insert element which must be verified by the design professional. Shear design values in this report for the Hangermate+ with an internally threaded head are for threaded rod or steel inserts with an ultimate strength,  $F_u \ge 125$  ksi; threaded rod or steel inserts with an  $F_u$  less than 125 ksi are allowed provided the steel strength shear values are multiplied by the ratio of  $F_u$  (ksi) of the steel insert and 125 ksi.
- **5.12** Prior to installation, calculations and details demonstrating compliance with this report must be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- **5.13** Since an ICC-ES acceptance criteria for evaluating data to determine the performance of anchors subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- **5.14** The <sup>1</sup>/<sub>4</sub>-inch- to <sup>3</sup>/<sub>4</sub>-inch-diameter (6.4 mm to 19.1 mm) Screw-Bolt+ anchors and <sup>1</sup>/<sub>4</sub>-inch-and <sup>3</sup>/<sub>8</sub>-inch-diameter (6.4 mm and 9.5 mm) Hangermate+ anchors may be installed in regions of concrete where cracking has occurred or where analysis indicates cracking may occur ( $f_t > f_r$ ), subject to the conditions of this report.
- **5.15** The  $^{1}/_{4}$ -inch- to  $^{3}/_{4}$ -inch-diameter (6.4 mm to 19.1 mm) Screw-Bolt+ anchors and  $^{1}/_{4}$ -inch-and  $^{3}/_{8}$ -inch-diameter (6.4 mm and 9.5 mm) Hangermate+ anchors may be used to resist short-term loading due to wind or seismic forces (Seismic Design Categories A through F under the IBC), subject to the conditions of this report.
- **5.16** Anchors are not permitted to support fire-resistance-rated construction. Where not otherwise prohibited by code, Screw-Bolt+ and Hangermate+ anchors are permitted for installation in fire-resistance-rated construction provided that at least one of the following conditions is fulfilled:

- Anchors are used to resist wind or seismic forces only.
- Anchors that support a fire-resistance-rated envelope or a fire-resistance-rated membrane, are protected by approved fire-resistance-rated materials, or have been evaluated for resistance to fire exposure in accordance with recognized standards.
- Anchors are used to support nonstructural elements.
- **5.17** Anchors have been evaluated for reliability against brittle failure and found to be not significantly sensitive to stress-induced hydrogen embrittlement.
- **5.18** Use of carbon steel anchors with zinc plating in accordance with ASTM B633 as described in Section 3.1 and 3.2 of this report is limited to dry, interior locations.
- **5.19** Special inspection must be provided in accordance with Section 4.4.
- **5.20** Screw-Bolt+ and Hangermate+ are manufactured under an approved quality control program with inspections by ICC-ES.

#### 6.0 EVIDENCE SUBMITTED

**6.1** Data in accordance with the ICC-ES Acceptance Criteria for Mechanical Anchors in Concrete Elements (AC193), dated October 2015, which incorporates requirements in ACI 355.2-07 / ACI 355.2-04, for use in cracked and uncracked concrete; including Test No. 11 (AC193, Annex 1, Table 4.2) for reliability of screw anchors against brittle failure, and optional service-condition Test No. 18 and Test No. 19 (AC193, Annex 1, Table 4.2) for seismic tension and shear.

6.2 Quality control documentation.

#### 7.0 IDENTIFICATION

- 7.1 The Screw-Bolt+ and Hangermate+ screw anchors are identified in the field by dimensional characteristics and packaging. A diameter and length marking is stamped on the hex head of each Screw-Bolt+ screw anchor; these are visible after installation for verification. Packages are identified with the company name as set forth in Section 3.1 of this report; anchor name; part number; type; anchor size and length; and the evaluation report number (ESR-3889).
- **7.2** The report holder's contact information is the following:

DEWALT 701 EAST JOPPA ROAD TOWSON, MARYLAND 21286 (800) 524-3244 <u>www.dewalt.com</u> <u>anchors@dewalt.com</u>

**7.3** The additional listee's contact information is the following:

THE HILLMAN GROUP 10590 HAMILTON AVENUE CINCINNATI, OHIO 45231 info@hillmangroup.com



The DEWALT drilling systems shown below collect and remove dust with a HEPA dust extractor during the hole drilling operation in dry base materials using hammer-drills (see step 1 of the manufacturer's published installation instructions).

FIGURE A-EXAMPLES OF DEWALT DUST REMOVAL DRILLING SYSTEMS WITH HEPA DUST EXTRACTORS FOR ILLUSTRATION

	Ins	tallation		Ten	sion Design Da	ita		Shear Design Da	ata
Product Name	Spec	ifications	Concret	е Тор	o of Steel Deck	Steel Deck Soffit	Concrete	Top of Steel Deck	Steel Deck Soffit
Screw-Bolt+	Tables	s 1, 2 and 5	Table 3	3	Table 3	Table 5	Table 4	Table 4	Table 5
Hangermate+	Tabl	e 1 and 5	Table 3	3	Table 3	Table 5	Table 4	Table 4	Table 5
Concrete Ty	ре	Concrete	e State		Anchor No	minal Size		Seismic Design (	Categories <sup>2</sup>
Normal-weight	and	Crack	ked		<sup>1</sup> / <sub>4</sub> ", <sup>3</sup> / <sub>8</sub> ", <sup>1</sup> /	2", <sup>5</sup> /8", <sup>3</sup> /4"		A through	۱F
lightweight		Uncrad	cked		<sup>1</sup> / <sub>4</sub> ", <sup>3</sup> / <sub>8</sub> ", <sup>1</sup> /	2", <sup>5</sup> /8", <sup>3</sup> /4"		A through	۱F

TABLE A-INSTALLATION AND DESIGN INDEX<sup>1</sup>

For SI: 1 inch = 25.4 mm. For **pound-inch** units: 1 mm = 0.03937 inch.

<sup>1</sup>Reference ACI 318-14 17.3.1.1 or ACI 318-11 D.4.1.1, as applicable. The controlling strength is decisive from all appropriate failure modes (i.e. steel, concrete breakout, pullout, pryout, as applicable) and design assumptions.

<sup>2</sup>See Section 4.1.8 for requirements for seismic design, where applicable.

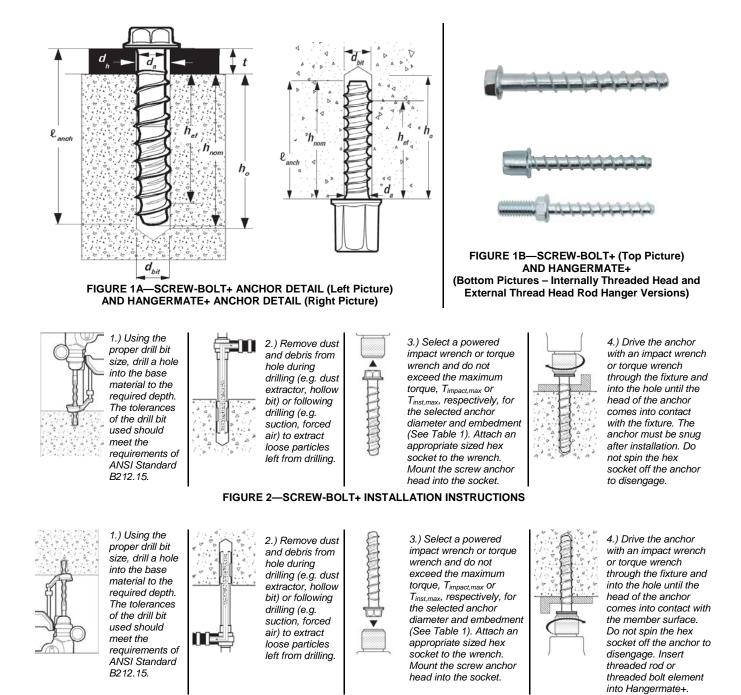


FIGURE 3—HANGERMATE+ INSTALLATION INSTRUCTIONS (Internally Threaded Rod Hanger Version Illustrated)

oltage (measured	** Maximum initial battery voltage (measured	** Maxin		Maximum <b>Optimum</b> – (Not Recommended) without a workload) is 20 volts. Nominal voltage is 18	Optimum – (N kload) is 20 volts. No	Maximum 0 without a worklo	anchor is	length of the	published size	Design. The	gth for Strength	denotes sizes which are less than the minimum standard anchor length for Strength Design. The published size length of the anchor is measured from under the head.	are less than the minin er the head.	* denotes sizes which measured from unc
DWMT75125B	ı	ı	DW5812	DW5475	DW5455	DW5475	20	10	1-1/8"	3/4"	10"	3/4" x 10"		PFM1411880
DWMT75125B	I	i.	DW5810	DW5474	DW5455	DW5474	40	10	1-1/8"	3/4"	œ	3/4" x 8"	PFM1461850	PFM1411840
DWMT75125B	I	I	DW5810	DW5474	DW5453	DW5474	60	20	1-1/8"	3/4"	6"	3/4" x 6"	PFM1461800	PFM1411800
DWMT75125B	1	ı.	DW5810	DW5474	DW5453	DW5474	60	20	1-1/8"	3/4"	ហ្ន	3/4" x 5"		PFM1411760
DWMT75125B	I	I	DW5810	DW5474	DW5453	DW5474	60	20	1-1/8"	3/4"	4"	3/4" x 4"		*PFM1411720
DWMT75125B	i.	I.	DW5810	DW5474	DW5453	DW5474	60	20	1-1/8"	3/4"	ယ္ခ	3/4" x 3"		*PFM1411700
DWMT75104B	I.	I.	DW5806	DW5471	DW5447	DW5471	50	25	15/16"	5/8"	œ	5/8" x 8"	PFM1461680	PFM1411680
DWMT75104B	I	I	DW5806	DW5471	DW5446	DW5471	75	25	15/16"	5/8"	6"	5/8" x 6"	PFM1461640	PFM1411640
DWMT75104B	I.	I.	DW5806	DW5471	DW5446	DW5471	75	25	15/16"	5/8"	ភ្ន	5/8" x 5"	PFM1461600	PFM1411600
DWMT75104B	ı.	I.	DW5806	DW5471	DW5446	DW5471	100	25	15/16"	5/8"	4"	5/8" x 4"		PFM1411580
DWMT75104B	i.	i.	DW5806	DW5471	DW5446	DW5471	100	25	15/16"	5/8"	မ္	5/8" x 3"		*PFM1411540
DWMT75113B	I.	I.	I.	DW5438	DW5438	DW5538	100	25	3/4"	1/2"	œٍ	1/2" x 8"	PFM1461520	PFM1411520
DWMT75113B	I	ı	I	DW5438	DW5438	DW5538	75	25	3/4"	1/2"	6"	1/2" x 6"	PFM1461480	PFM1411480
DWMT75113B	1	I.	ı.	DW5438	DW5438	DW5538	100	25	3/4"	1/2"	പ്	1/2" x 5"	PFM1461460	PFM1411460
DWMT75113B	I	ī	ı	DW5437	DW5437	DW5537	150	50	3/4"	1/2"	4"	1/2" x 4"	PFM1461420	PFM1411420
DWMT75113B	1	1	1	DW5437	DW5437	DW5537	150	50	3/4"	1/2"	မ္	1/2" x 3"		PFM1411380
DWMT75113B	I	ı	I	DW5437	DW5437	DW5537	200	50	3/4"	1/2"	2-1/2"	1/2" x 2-1/2"		PFM1411360
DWMT75113B	I.	I.	i.	DW5437	DW5437	DW5537	200	50	3/4"	1/2"	2"	1/2" x 2"		*PFM1411340
I	DWMT75122B			DW5429	DW5429	DW5529	150	50	9/16"	3/8"	6"	3/8" x 6"	PFM1461320	PFM1411320
1	DWMT75122B	I	I	DW5429	DW5429	DW5529	250	50	9/16"	3/8"	ភ្ន	3/8" x 5"	PFM1461300	PFM1411300
I	DWMT75122B	ī		DW5427	DW5427	DW5527	250	50	9/16"	3/8"	4"	3/8" x 4"	PFM1461280	PFM1411280
T	DWMT75122B	i.	i.	DW5427	DW5427	DW5527	250	50	9/16"	3/8"	ယ္ခ	3/8" x 3"	PFM1461240	PFM1411240
I	DWMT75122B	ı	ı	DW5427	DW5427	DW5527	300	50	9/16"	3/8"	2-1/2"	3/8" x 2-1/2"		PFM1411220
i.	DWMT75122B	I.	I.	DW5427	DW5427	DW5527	300	50	9/16"	3/8"	1-3/4"	3/8" x 1-3/4"		*PFM1411160
L	i.	DWMT74479B	i.	DW5417	DW5417	DW5517	500	100	7/16"	1/4"	ယ္ခ	1/4" x 3"		PFM1411100
ı		DWMT74479B		DW5417	DW5417	DW5517	500	100	7/16"	1/4"	2-5/8"	1/4" x 2-5/8"		PFM1411080
I	I	DWMT74479B	I	DW:5417	DW5417	DW5517	600	100	7/16"	1/4"	2-1/4"	1/4" x 2-1/4"	•	PFM1411060
I	ı.	DWMT74479B	ı.	DW5417	DW5417	DW5517	600	100	7/16"	1/4"	1-3/4"	1/4" x 1-3/4"		PFM1411020
I.	I.	DWMT74479B	I.	DW5417	DW5417	DW5517	600	100	7/16"	1/4"	1-1/4"	1/4" x 1-1/4"		*PFM1411000
<b>(ETS</b>	IMPACT RATED SOCKETS	IMP		Carbide Bits	CARBI		MASTER	ΩΤΥ	SIZE	HOLE	LENGTH	ANCHOR	Galvanized	ZINC PLATED
													NUMBER	CATALOG NUMBER
DCF899P2 High Torque 1/2" (Speed #2)	DCF880M2 1/2" Impact Wrench	DCF883L2 3/8" Impact Wrench	DCH481X2 1-9/16" W/ E-Clutch	DCH293R2 1-1/8" L-Shape w/ E-Clutch	DCH133M2 1" D-Handle	DCH273P2DH 1" L-Shape								
ENCHES	20V MAX** IMPACT WRENCHES	20V M/	Flexvolt SDS Max	RY HAMMERS	20V MAX** SDS PLUS ROTARY HAMMERS	20V MAX** S								

#### TABLE 1—SCREW-BOLT+ AND HANGERMATE+ ANCHOR INSTALLATION AND SUPPLEMENTAL INFORMATION<sup>1,2,4</sup>

	nahar	Bronorty /								Nomir	nal And	hor Si	ze (inc	:h)				
		Property / nformation	Notation	Units	1/	4	1/		6-	<sup>3</sup> / <sub>8</sub>		6-	<sup>1</sup> / <sub>2</sub> rew-Bo			<sup>5</sup> / <sub>8</sub> rew-Bo		<sup>3</sup> / <sub>4</sub> Screw-Bolt+
Head s	style		-	-	Hanger Threa		Screw-			<mark>rew-Bo</mark> ex Hea			<mark>rew-во</mark> ex Hea			ex Не		Hex Head
		or diameter	da	in.	0.2		0.2	50		0.375			0.500			0.625		0.750
		neter of hole		(mm) in.	(6.	,	(6. <sup>3</sup> /			(9.5) <sup>1</sup> / <sub>2</sub>			(12.7) <sup>5</sup> / <sub>8</sub>			(15.9) <sup>3</sup> / <sub>4</sub>		(19.1) <sup>7</sup> / <sub>8</sub>
cleara	nce in f	ixture	d <sub>h</sub>	(mm)	N/		(9.	5)		(12.7)			(15.9)		5	(19.1)		(22.2)
-		bit diameter	d <sub>bit</sub>	in.	<sup>1</sup> / <sub>4</sub> A		<sup>1</sup> / <sub>4</sub> A			/ <sub>8</sub> ANS			/2 ANS			/ <sub>8</sub> ANS		<sup>3</sup> / <sub>4</sub> ANSI
	um non Iment c		h <sub>nom</sub>	in. (mm)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)	3 <sup>1</sup> / <sub>4</sub> (83)	2 <sup>1</sup> / <sub>2</sub> (64)	3 (76)	4 <sup>1</sup> / <sub>4</sub> (108)			5 (127)	4 <sup>1</sup> / <sub>4</sub> (108)
Effecti	ve emb	edment	h <sub>ef</sub>	in. (mm)	1.20 (30)	1.94 (49)	1.20 (30)	1.94 (49)	1.33 (33)	1.75 (44)	2.39 (60)	1.75 (44)	2.17 (55)	3.23 (82)	2.24 (56)	2.88 (73)	3.73 (94)	3.08 (78)
Minim	um hole	e depth	h <sub>o</sub>	in. mm	2 (51)	$\frac{2^{7}}{8}$ (73)	2 (51)	$\frac{2^{7}}{8}$ (73)	$2^{3}/_{8}$ (60)	2 <sup>7</sup> / <sub>8</sub> (73)	3 <sup>5</sup> / <sub>8</sub> (92)	2 <sup>7</sup> / <sub>8</sub> (73)	3 <sup>3</sup> / <sub>8</sub> (86)	4 <sup>5</sup> / <sub>8</sub> (117)	3 <sup>5</sup> / <sub>8</sub> (86)	4 <sup>3</sup> / <sub>8</sub> (111)	5 <sup>3</sup> / <sub>8</sub> (137)	4 <sup>5</sup> / <sub>8</sub> (117)
Minimu thickne		crete member	h <sub>min</sub>	in. (mm)	3 <sup>1</sup> / <sub>4</sub> (83)	4 (102)	3 <sup>1</sup> / <sub>4</sub> (83)	4 (102)	3 <sup>1</sup> / <sub>2</sub> (89)	4 (102)	5	$\frac{4^{1}}{(114)}$	5 <sup>1</sup> / <sub>4</sub> (133)	$6^{3}/_{4}$ (171)	5 (127)	6 (152)	7 (178)	6 (152)
Minim	um edg	e distance <sup>6</sup>	C <sub>min</sub>	in. (mm)	(30)	/2	1 <sup>1</sup> (3)	/2	Cmin	$= 1^{1}/_{2}$ min $\geq 3$	(38)	( ,	$1^{3}/_{4}$ (44)	()	()	$1^{3}/_{4}$ (44)	(	1 <sup>3</sup> / <sub>4</sub> (44)
Minim	um spa	cing distance <sup>6</sup>	S <sub>min</sub>	in.	1 <sup>1</sup>	/2	1 <sup>1</sup>	/2	Sm	in = 2 (!	51)		$2^{3}/_{4}$			$2^{3}/_{4}$		3
o				(mm) in.	(3) 4.3	5) 6.1	(3 4.3	6.1	5.0	<sub>min</sub> ≥ 2 6.3	7.8	3.3	(70) 5.9	8.1	6.3	(70) 7.9	10.1	(76) 10.9
		distance	C <sub>ac</sub>	(mm)	(110)	(156)	(110)	(156)	(127)	(160)	(198)	(83)	(150)	(205)	(159)	(201)	(255)	(277)
	um non r length		$\ell_{\mathit{anch}}$	in. (mm)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	1 <sup>3</sup> / <sub>4</sub> (44)	3 (76)	2 <sup>1</sup> / <sub>2</sub> (64)	3 (76)	4 (102)	3 (76)	4 (102)	5 (127)	4 (102)	5 (127)	6 (152)	6 (152)
	ium imp (torque	bact wrench	T <sub>impact,max</sub>	ftlb. (N-m)	15 (20		15 (20			300 (407)			300 (407)			700 (949)		700 (949)
Max. ir	nstallati	ion torque	T <sub>inst,max</sub>	ftlb. (N-m)	19 <sup>[3]</sup> (26)	25 (34)	19 <sup>[3]</sup> (26)	25 (34)		5 4)	40 (54)	45 60 (61) (81)			60 (81)		70 (81)	
ad	Wrenc	h socket size	$\frac{1}{4}$ " thread	in.	3/ 1/	8			,	,		,	,		(01)			
He			3/8" thread $1/4$ " thread		33	2 / <sub>64</sub>												
Internally Threaded Head	Max. h	nead height	<sup>3</sup> / <sub>8</sub> " thread	in.	43	/64	N	I/A		N/A			N/A		N/A			N/A
ln Thre	Max. v	vasher dia.	$\frac{1}{4}$ " thread $\frac{3}{8}$ " thread	in.	1	/ <sub>2</sub> / <sub>32</sub>												
g	Wrenc	h socket size	78 thead			/32 /2												
External read Hea		nead height	<sup>3</sup> / <sub>8</sub> " thread	in.			N	I/A		N/A			N/A			N/A		N/A
External Thread Head	(includ	ling thread)	78 theat			<sup>3</sup> / <sub>16</sub>		/A		IN/A			IN/A			IN/A		IN/A
F		vasher dia.	-		21	/32	7	/ <sub>16</sub>		<sup>9</sup> / <sub>16</sub>			<sup>3</sup> / <sub>4</sub>			<sup>15</sup> / <sub>16</sub>		1 <sup>1</sup> /8
ad x		h socket size		in.			21	/16 / <sub>64</sub>		<sup>3</sup> / <sub>8</sub>			<sup>31</sup> / <sub>64</sub>			<sup>37</sup> / <sub>64</sub>		<sup>43</sup> / <sub>64</sub>
Hex Head		head height	-	in.	N	/A	37	/ <sub>64</sub> / <sub>64</sub>		<sup>3</sup> / <sub>4</sub>			1 <sup>1</sup> / <sub>16</sub>			1 <sup>1</sup> / <sub>8</sub>		1 <sup>13</sup> / <sub>32</sub>
Effectiv		vasher dia.	-	in. in. <sup>2</sup>	0.0	45	0.0	/64 /6		0.094			0.176			0.274		0.399
		ile stress area r body)	A <sub>se</sub>	(mm <sup>2</sup> )	(28		(28			(60.7)			(113.9)			(177.0)		(257.2)
Minimu streng		cified ultimate	f <sub>uta</sub>	psi (N/mm <sup>2</sup> )	100, (69		100, (69			92,500 (638)	)		115,000 (793)	)		95,000 (658)	)	95,000 (658)
U	um spe	cified yield	f <sub>ya</sub>	psi (N/mm <sup>2</sup> )	80,0 (55	000	80,0 (55	000		74,000 (510)	1		92,000 (634)			76,000		76,000 (524)
J		Uncracked	β <sub>uncr</sub>	lbf/in.	1,381	,000	1,252	,000	1	,157,00	00	1	,014,00	0	(524) 919,000			1,028,000
Mean stiffnes		concrete Cracked	β <sub>cr</sub>	(kN/mm) lbf/in.	(23 318,	000	(21 355,	000	;	(195) 330,000	C	;	(171) (155) 349,000 378,000		0	(173) 419,000		
		concrete	1201	(kN/mm)	(54	4)	(60	,		(56)			(59)			(64)		(71)

For SI: 1 inch = 25.4 mm, 1 ft-lb = 1.356 N-m, 1 psi = 0.0069 N/mm<sup>2</sup> (MPa).

N/A = Not Applicable.

<sup>1</sup>The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable. <sup>2</sup>For installations in the topside of concrete-filled steel deck assemblies with minimum concrete member thickness,  $h_{min,deck_1}$  of 2.5 inches above the

upper flute (topping thickness). See Table 2 and the installation detail in Figure 4 of this report.

<sup>3</sup>For installations in the topside of concrete-filled steel deck assemblies with sand-lightweight concrete fill, the maximum installation torque, T<sub>instmax</sub>, is 18 ft -lb

<sup>4</sup>For installations through the soffit of steel deck assemblies into concrete, see Table 5 and the installation detail in Figures 5A, 5B, 6A and 6B of this report. Tabulated minimum spacing values are based on anchors installed along the flute with axial spacing equal to the greater of 3her or 1.5 times the flute width.

<sup>5</sup>The embedment depth, *h<sub>nom</sub>* is measured from the outside surface of the concrete member to the embedded end of the anchor.

<sup>6</sup>Additional combinations for minimum edge distance, c<sub>min</sub>, and minimum spacing distance, s<sub>min</sub>, may be derived by linear interpolation between the given boundary values for the 3/8-inch-diameter anchors.

The listed minimum anchor length is based on the anchor sizes commercially available at the time of publication compared with the requirements to achieve the minimum nominal embedment depth, including consideration of a fixture attachment for hex head anchors. The minimum nominal anchor length is measured from under the head to the tip of the anchor.

<sup>8</sup>Mean values shown, actual stiffness varies considerably depending on concrete strength, loading and geometry of application.

#### TABLE 2—ANCHOR SETTING INFORMATION FOR INSTALLATION ON THE TOP OF CONCRETE-FILLED STEEL DECK ASSEMBLIES WITH MINIMUM TOPPING THICKNESS<sup>1,2,3,4</sup>

Anchor Property /				1	Nominal Anchor Size (inch)	
Setting Information	Notation	Units		/ <sub>4</sub> r-Bolt+	<sup>3</sup> / <sub>8</sub> Screw-Bolt+	<sup>1</sup> / <sub>2</sub> Screw-Bolt+
Head style	-	-	Hex	Head	Hex Head	Hex Head
Nominal anchor diameter	da	in. (mm)	(6	250 .4)	0.375 (9.5)	0.500 (12.7)
Minimum diameter of hole clearance in fixture	d <sub>h</sub>	in. (mm)		/ <sub>8</sub> .5)	1/2 (12.7)	<sup>5</sup> / <sub>8</sub> (15.9)
Nominal drill bit diameter	d <sub>bit</sub>	in.	<sup>1</sup> / <sub>4</sub> A	NSI	<sup>3</sup> / <sub>8</sub> ANSI	<sup>1</sup> / <sub>2</sub> ANSI
Minimum nominal embedment depth <sup>5</sup>	h <sub>nom</sub>	in. (mm)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)
Effective embedment	h <sub>ef</sub>	in. (mm)	1.20 (30)	1.94 (49)	1.33 (33)	1.75 (44)
Minimum hole depth	h <sub>o</sub>	in. mm	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)	2 <sup>3</sup> / <sub>8</sub> (60)	2 <sup>1</sup> / <sub>2</sub> (64)
Minimum concrete member thickness (topping thickness)	h <sub>min,deck</sub>	in. (mm)	2 <sup>1</sup> / <sub>2</sub> (64)	2 <sup>1</sup> / <sub>2</sub> (64)	2 <sup>1</sup> / <sub>2</sub> (64)	2 <sup>1</sup> / <sub>2</sub> (64)
Minimum edge distance	C <sub>min, deck, top</sub>	in. (mm)		<sup>1</sup> / <sub>2</sub> 88)	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)
Minimum spacing distance	Smin, deck, top	in. (mm)		<sup>1</sup> / <sub>2</sub> 88)	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)
Critical edge distance	Cac,deck,top	in. (mm)	3.0 (76)	4.0 (102)	3.5 (89)	6.0 (152)
Minimum nominal anchor length <sup>6</sup>	$\ell_{\mathit{anch}}$	in. (mm)	1 <sup>3</sup> / <sub>4</sub> (44)	3 (76)	2 <sup>1</sup> / <sub>2</sub> (64)	3 (76)
Maximum impact wrench power (torque)	T <sub>impact,max</sub>	ftlb. (N-m)		50 03)	300 (407)	300 (407)
Max. installation torque	T <sub>inst,max</sub>	ftlb. (N-m)	18(26)	25 (34)	25 (34)	45 (61)
Wrench socket size	-	in.	7	/ <sub>16</sub>	<sup>9</sup> / <sub>16</sub>	3/4
Max. head height	-	in.	2	<sup>1</sup> / <sub>64</sub>	<sup>3</sup> / <sub>8</sub>	<sup>31</sup> / <sub>64</sub>
Max. washer diameter	-	in.	3	<sup>7</sup> / <sub>64</sub>	<sup>3</sup> / <sub>4</sub>	1 <sup>1</sup> / <sub>16</sub>

For **SI:** 1 inch = 25.4 mm, 1 ft-lbf = 1.356 N-m.

<sup>1</sup>The anchors may be installed in the topside of concrete-filled steel deck floor and roof assemblies in accordance with Section 4.3 of this report provided the concrete thickness above the upper flute meets the minimum thicknesses specified in this table. Minimum concrete member thickness, hmin.deck, refers to the concrete thickness above the upper flute (topping thickness). See Figure 4 of this report. <sup>2</sup>Applicable to the following conditions:

For  $\frac{1}{4}$ -inch-diameter anchors with  $1^{5}/_{8}$ -inch nominal embedment,  $2^{1}/_{2}$ -inch  $\leq h_{min,deck} < 3^{1}/_{4}$ -inch.

For  $\frac{1}{4}$ -inch-diameter anchors with  $2^{1}/_{2}$ -inch nominal embedment,  $2^{1}/_{2}$ -inch  $\leq h_{min,deck} < 4$ -inch.

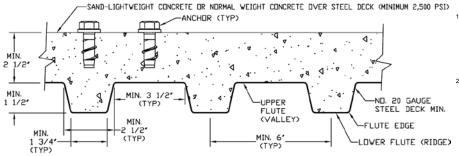
For  $\frac{3}{8}$ -inch-diameter anchors with 2-inch nominal embedment,  $\frac{2}{2}$ -inch  $\leq h_{min,deck} < \frac{3}{2}$ -inch.

For  $\frac{1}{2}$ -inch-diameter anchors with  $\frac{2}{2}$ -inch nominal embedment,  $\frac{2}{2}$ -inch  $\leq h_{min,deck} < \frac{4}{2}$ -inch.

<sup>3</sup>For all other anchor diameters and embedment depths, refer to Table 1 for applicable values of h<sub>min</sub>, c<sub>min</sub> and s<sub>min</sub>, which can be substituted for h<sub>min,deck</sub>, *C<sub>min,deck,top</sub>* and *S<sub>min,deck,top</sub>*, respectively.
 <sup>4</sup>Design capacities shall be based on calculations according to values in Tables 3 and 4 of this report.

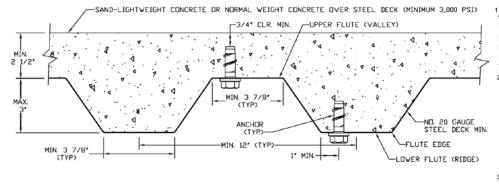
<sup>5</sup>The embedment depth, *h<sub>nom</sub>* is measured from the outside surface of the concrete member to the embedded end of the anchor.

<sup>6</sup>The listed minimum overall anchor length is based on the anchor sizes commercially available at the time of publication compared with the requirements to achieve the minimum nominal embedment depth, including consideration of a fixture attachment for hex head anchors. The minimum nominal anchor length is measured from under the head to the tip of the anchor.



<sup>1</sup>Anchors may be placed in the top side of concrete over steel deck profiles in accordance with Figure 4 provided the minimum concrete thickness above the upper flute (topping thickness), minimum spacing distance and minimum edge distances are satisfied as given in Table 2 of this report. <sup>2</sup>For all other anchor diameters and embedment depths installed in the top of concrete over steel deck profiles with topping thickness greater than or equal to the minimum concrete member thicknesses given in Table 1, the minimum spacing distances and minimum edge distances must be used from Table 1, as applicable.

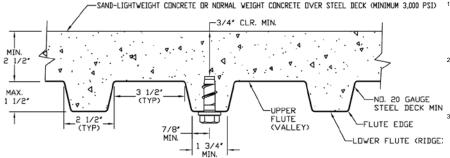
FIGURE 4—INSTALLATION DETAIL FOR ANCHORS IN THE TOP OF CONCRETE OVER STEEL DECK FLOOR AND ROOF ASSEMBLIES WITH MINIMUM TOPPING THICKNESS (SEE DIMENSIONAL PROFILE REQUIREMENTS)<sup>1,2</sup>



<sup>1</sup>Anchors may be placed in the upper flute or lower flute of concrete-filled steel deck profiles in accordance with Figure 5A provided the minimum hole clearance of  ${}^{3}$ /<sub>4</sub>inch is satisfied for the selected anchor. See Table 5.

<sup>2</sup>Anchors in the lower flute of Figure 5A profiles may be installed with a maximum <sup>15</sup>/<sub>16</sub>-inch offset in either direction from the center of the flute. The offset distance may be increased proportionally for profiles with lower flute widths greater than those shown provided the minimum lower flute edge distance is also satisfied (e.g.  $1^{1}/_{4}$ -inch offset for  $4^{1}/_{2}$ -inch wide flute). <sup>3</sup>See Table 5 of this report for design data.

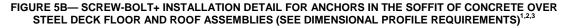
#### FIGURE 5A—SCREW-BOLT+ INSTALLATION DETAIL FOR ANCHORS IN THE SOFFIT OF CONCRETE OVER STEEL DECK FLOOR AND ROOF ASSEMBLIES (SEE DIMENSIONAL PROFILE REQUIREMENTS)<sup>1,2,3</sup>

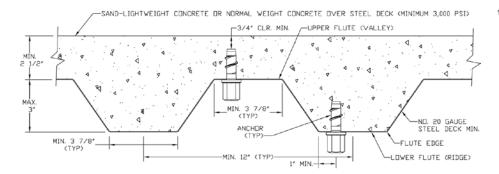


<sup>1</sup>Anchors may be placed in the upper flute or lower flute of the concrete-filled steel deck profiles in accordance with Figure 5B provided the minimum hole clearance of  ${}^{3}$ /<sub>4</sub>-inch is satisfied for the selected anchor. See Table 5.

<sup>2</sup>Anchors in the lower flute of Figure 5B profiles may be installed in the center of the flute. An offset distance may be given proportionally for profiles with flute widths greater than those shown provided the minimum lower flute edge distance is also satisfied.

<sup>3</sup>See Table 5 of this report for design data.

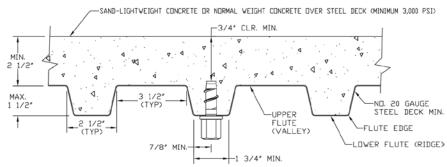




<sup>1</sup>Anchors may be placed in the upper flute or lower flute of the concrete-filled steel deck profiles in accordance with Figure 6A provided the minimum hole clearance of <sup>3</sup>/<sub>4</sub>-inch is satisfied for the selected anchor. See Table 5.

<sup>2</sup>Anchors in the lower flute of Figure 6A profiles may be installed with a maximum  $^{15}/_{16}$ -inch offset in either direction from the center of the flute. The offset distance may be increased proportionally for profiles with lower flute widths greater than those shown provided the minimum lower flute edge distance is also satisfied (e.g.  $1^{1}/_{4}$ - inch offset for  $4^{1}/_{2}$ -inch wide flute). <sup>3</sup>See Table 5 of this report for design data.

FIGURE 6A—HANGERMATE+ INSTALLATION DETAIL FOR SCREW ANCHORS IN THE SOFFIT OF CONCRETE OVER STEEL DECK FLOOR AND ROOF ASSEMBLIES (SEE DIMENSIONAL PROFILE REQUIREMENTS)<sup>1,2,3</sup>



<sup>1</sup>Anchors may be placed in the upper flute or lower flute of the concrete-filled steel deck profiles in accordance with Figure 6B provided the minimum hole clearance of  ${}^{9}_{4}$ -inch is satisfied for the selected anchor. See Table 5.

<sup>2</sup>Anchors in the lower flute of Figure 6B profiles may be installed in the center of the flute. An offset distance may be given proportionally for profiles with flute widths greater than those shown provided the minimum lower flute edge distance is also satisfied.

<sup>3</sup>See Table 5 of this report for design data.

FIGURE 6B—HANGERMATE+ INSTALLATION DETAIL FOR SCREW ANCHORS IN THE SOFFIT OF CONCRETE OVER STEEL DECK FLOOR AND ROOF ASSEMBLIES (SEE DIMENSIONAL PROFILE REQURIEMENTS)<sup>1,2,3</sup>

#### TABLE 3—TENSION DESIGN INFORMATION FOR SCREW-BOLT+ AND HANGERMATE+ SCREW ANCHORS IN CONCRETE<sup>1.2,9</sup>

Anchor Property /								Nom	inal Ar	nchor \$	Size (ir	nch)				
Setting Information	Notation	Units	<sup>1</sup> / Hanger			/ <sub>4</sub> /-Bolt+	Sc	<sup>3</sup> / <sub>8</sub> rew-Bo	olt+	Sc	<sup>1</sup> / <sub>2</sub> rew-Bo	lt+	Sc	<sup>5</sup> / <sub>8</sub> crew-Bo	olt+	<sup>3</sup> / <sub>4</sub> Screw-Bolt+
Anchor category	1, 2 or 3	-	1			1		1			1			1		1
Head style	-	-	Threa	aded	Hex	Head	F	lex Hea	ıd	Η	lex Hea	d	ŀ	Hex Hea	ıd	Hex Head
Minimum nominal embedment depth	h <sub>nom</sub>	in. (mm)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)	3 <sup>1</sup> / <sub>4</sub> (83)	2 <sup>1</sup> / <sub>2</sub> (64)	3 (76)	4 <sup>1</sup> / <sub>4</sub> (108)	3 <sup>1</sup> / <sub>4</sub> (83)	4 (102)	5 (127)	4 <sup>1</sup> / <sub>4</sub> (108)
	STE	EL STI	RENGT	H IN TE	ENSIO	N (ACI	318-14	17.4.1	l or AC	CI 318-'	11 D.5.	1)				
Steel strength in tension	N <sub>sa</sub>	lb (kN)	4,5 (20			535 ).2)		8,730 (38.8)			20,475 (91.1)			26,260 (116.8)		38,165 (169.8)
Reduction factor, steel strength <sup>3,4</sup>	$\phi$	-	0.6	65	0.	65		0.65			0.65			0.65		0.65
CO	NCRETE I	BREAK	OUT S	TRENG	STH IN	TENS	ON (A	CI 318	-14 17.	4.2 or	ACI 31	8-11 D	).5.2)			
Effective embedment	h <sub>ef</sub>	in. (mm)	1.20 (30)	1.94 (49)	1.20 (30)	1.94 (49)	1.33 (33)	1.75 (44)	2.39 (60)	1.75 (44)	2.17 (55)	3.23 (82)	2.24 (56)	2.88 (73)	3.73 (94)	3.08 (78)
Critical edge distance	C <sub>ac</sub>	in. (mm)	4.3 (110)	6.1 (156)	4.3 (110)	6.1 (156)	5.0 (127)	6.3 (160)	7.8 (298)	3.3 (83)	5.9 (150)	8.1 (205)	6.3 (159)	7.9 (201)	10.1 (255)	10.9 (277)
Critical edge distance, topside of concrete-filled steel decks with minimum topping thickness <sup>9</sup>	Cac,deck,top	in. (mm)	_ [11]	- [11]	3.0 (76)	4.0 (102)	3.5 (89)	_ [11]	- [11]	6.0 (152)	_ [11]	_ [11]	- [11]	_ [11]	- [11]	_ [11]
Effectiveness factor for uncracked concrete	k <sub>uncr</sub>	-	27	24	27	24	30	2	4	30	30 24		30	24	4	27
Effectiveness factor for cracked concrete	k <sub>cr</sub>	-	17	7	1	7		17			17			21		17
Modification factor, cracked and uncracked concrete <sup>5</sup>	$\Psi_{c,N}$	-	1.	0	1	.0		1.0			1.0			1.0		1.0
Reduction factor, concrete breakout strength <sup>3</sup>	$\phi$	-	0.6	85	0.	65		0.65			0.65			0.65		0.65
	PULL	OUT S	TRENG	TH IN 1	TENSI	ON (AC	318- <sup>-</sup>	14 17.4	l.3 or A	ACI 318	3-11 D.	5.3)				
Pullout strength, uncracked concrete (2,500 psi) <sup>6,10</sup>	N <sub>p,uncr</sub>	lb (kN)	See n	ote 7	See r	note 7	S	ee note	7	S	ee note	7	s	ee note	7	See note 7
Pullout strength, cracked concrete (2,500 psi) <sup>6,10</sup>	N <sub>p,cr</sub>	lb (kN)	765 (3.4)	1,415 (6.3)	765 (3.4)	1,415 (6.3)	S	ee note	7	1,645 (7.3)	2,515 (11.2)	4,700 (20.9)		4,720 (21.0)	6,900 (30.7)	See note 7
Reduction factor, pullout strength <sup>3</sup>	$\phi$	-	0.6	65	0.	65		0.65			0.65			0.65		0.65
PULLOUT ST	RENGTH	IN TEN	ISION F	OR SE	ISMIC	APPL	CATIC	NS (A	CI 318	-14 17.	2.3.3 o	r ACI :	318-11	D.3.3.	3)	
Pullout strength, seismic (2,500 psi) <sup>6,8,10</sup>	N <sub>p,eq</sub>	lb (kN)	360 (1.6)	1,170 (5.2)	360 (1.6)	1,170 (5.2)	900 (4.0)	,	2,765 (12.3)	,	2,515 (11.2)			2,445 (10.9)	3,370 (15.0)	4,085 (18.2)
Reduction factor, pullout strength, seismic <sup>3</sup>	$\phi$	-	0.6	65	0.	65		0.65			0.65			0.65		0.65

For SI: 1 inch = 25.4 mm, 1 ft-lb = 1.356 N-m, 1 psi = 0.0069 N/mm<sup>2</sup> (MPa).

<sup>1</sup>The data in this table is intended to be used with the design provisions of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable; for anchors resisting seismic load combinations the additional requirements of ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable, shall apply.

<sup>2</sup>Installation must comply with manufacturer's published installation instructions and details.

<sup>3</sup>All values of  $\phi$  were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3, or ACI 318-11 Section 9.2. If the load combinations of ACI 318-11 Appendix C are used, then the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4. For reinforcement that complies with ACI 318-14 Chapter 17 or ACI 318-11 Appendix D requirements for Condition A, see ACI 318-14 17.3.3(c) or ACI 318-11 Section D.4.3(c), as applicable for the appropriate  $\phi$  factor when the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used.

<sup>4</sup>The anchors are considered a brittle steel elements as defined by ACI 318-14 2.3 or ACI 318-11 D.1, as applicable.

<sup>5</sup>Select the appropriate effectiveness factor for cracked concrete ( $k_{cr}$ ) or uncracked concrete ( $k_{uncr}$ ) and use  $\psi_{c,N} = 1.0$ .

<sup>6</sup>For calculation of  $N_{pn}$  see Section 4.1.4 of this report. The characteristic pullout strength for concrete compressive strengths greater than 2,500 psi for <sup>1</sup>/<sub>4</sub>-inch-diameter anchors may be increased by multiplying the value in the table by  $(f'_c / 2,500)^{0.3}$  for psi or  $(f'_c / 17.2)^{0.3}$  for MPa. The characteristic pullout strength for concrete compressive strengths greater than 2,500 psi for <sup>3</sup>/<sub>8</sub>-inch- to <sup>3</sup>/<sub>4</sub>-inch-diameter anchors may be increased by multiplying the value in the table by  $(f'_c / 2,500)^{0.3}$  for psi or  $(f'_c / 17.2)^{0.5}$  for MPa. The characteristic pullout strength for concrete compressive strengths greater than 2,500 psi for <sup>3</sup>/<sub>8</sub>-inch- to <sup>3</sup>/<sub>4</sub>-inch-diameter anchors may be increased by multiplying the value in the table by  $(f'_c / 2,500)^{0.5}$  for psi or  $(f'_c / 17.2)^{0.5}$  for MPa.

<sup>7</sup>Pullout strength does not control design of indicated anchors and does not need to be calculated for indicated anchor size and embedment.

<sup>8</sup>Reported values for characteristic pullout strength in tension for seismic applications are based on test results per ACI 355.2, Section 9.5.

<sup>9</sup>Anchors are permitted in the topside of concrete-filled steel deck assemblies in accordance with Figure 4 of this report.

<sup>10</sup>Anchors are permitted to be used in lightweight concrete in accordance with Section 4.1.12 of this report.

<sup>11</sup>Tabulated critical edge distance values,  $C_{ac,deck,top}$  are for anchors installed in the top of concrete over steel deck profiles with a minimum concrete thickness,  $h_{min,deck}$  of 2.5 inches above the upper flute (topping thickness). For minimum topping thickness greater than or equal to the minimum concrete member thicknesses,  $h_{min}$  given in Table 1, the associated critical edge distance,  $c_{ac}$  for indicated anchor diameters and embedment depths may be used in the calculation of  $\Psi_{cp,N}$  in accordance with Section 4.1.10 of this report, as applicable.

#### TABLE 4—SHEAR DESIGN INFORMATION FOR SCREW-BOLT+ AND HANGERMATE+ SCREW ANCHORS IN CONCRETE<sup>1,2,7,8,9</sup>

Anchor Property /						Nominal	Ancho	or Size (incl	ı)				
Setting Information	Notation	Units	Hang	<sup>1</sup> / <sub>4</sub> ermate+	<sup>1</sup> / <sub>4</sub> Screw-Bolt+	<sup>3</sup> / <sub>8</sub> Screw-B	olt+	<sup>1</sup> / <sub>2</sub> Screw-E	olt+	So	⁵/ <sub>8</sub> crew-Bo	olt+	<sup>3</sup> / <sub>4</sub> Screw-Bolt+
Anchor category	1, 2 or 3	-		1	1	1		1			1		1
Head style	-	-	Thr	readed	Hex Head	Hex He	ad	Hex He	ad	ł	Hex Hea	ad	Hex Head
Threaded diameter	-	in.	<sup>1</sup> / <sub>4</sub>	<sup>3</sup> /8	N/A	N/A		N/A			N/A		N/A
Minimum nominal embedment depth	h <sub>nom</sub>	in. (mm)	1 <sup>5</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>2</sub> (41) (64)	$\begin{array}{c c} 1^{5}\!/_{8} & 2^{1}\!/_{2} \\ (41) & (64) \end{array}$	$\begin{array}{c c} 1^{5}\!/_{8} & 2^{1}\!/_{2} \\ (41) & (64) \end{array}$	$\begin{array}{c c} 2 & 2^{1}/_{2} \\ (51) & (64) \end{array}$	3 <sup>1</sup> / <sub>4</sub> (83)	$ \begin{array}{c c} 2^{1}/_{2} & 3 \\ (64) & (76) \end{array} $	4 <sup>1</sup> / <sub>4</sub> (108)	3 <sup>1</sup> / <sub>4</sub> (83)	4 (102)	5 (127)	4 <sup>1</sup> / <sub>4</sub> (108)
		ST	TEEL STR	ENGTH IN SH	IEAR (ACI 31	8-14 17.5.1	or ACI	318-11 D.6	.1)				
Steel strength in shear <sup>5</sup>	V <sub>sa</sub>	lb (kN)	860 (3.8)	1,545 (6.9)	1,635 2,040 (7.3) (9.1)	3,465 (15.4)	4,345 (19.3)	8,860 (39.4)	11,175 (49.7)		,310 4.8)	15,585 (69.3)	19,260 (85.7)
Reduction factor, steel strength <sup>3,4</sup>	$\phi$	-	(	).60	0.60	0.60		0.60	)		0.60	•	0.60
ST	EEL STRE	NGTH	IN SHEAF	R FOR SEISM	IC APPLICA	FIONS (ACI	318-14	17.2.3.3 or	ACI 31	3-11 D	.3.3.3)		
Steel strength in shear, seismic <sup>6</sup>	V <sub>sa,eq</sub>	lb (kN)	600 (2.7)	1,390 (6.2)	1,360 1,700 (6.1) (7.6)	2,415 (10.8)	3,030 (13.5)	7,090 (31.5)	8,940 (39.8)		845 3.8)	12,465 (55.5)	15,405 (68.5)
Reduction factor, steel strength, seismic <sup>3</sup>	$\phi$	-	(	0.60	0.60	0.60	•	0.60			0.60	•	0.60
	CON	CRET	E BREAKO	OUT STRENG	GTH IN SHEAR (ACI 318-14 17.5.)			5.2 or ACI 3	,			•	
Nominal anchor diameter	da	in. (mm)	-	.250 6.4)	0.250 (6.4)	0.375 (9.5)	0.50 (12.7	0.625 (15.9)			0.750 (19.1)		
Load bearing length of anchor	le	in. (mm)	1.20 1.94 (30) (49)	1.20 1.94 (30) (49)	1.20 1.94 (30) (49)	1.33 1.75 (33) (44)	2.39 (60)	1.75 2.17 (44) (55		2.24 (56)	2.88 (73)	3.73 (94)	3.08 (78)
Reduction factor, concrete breakout strength <sup>3</sup>	φ	-	(	).70	0.70	0.70	•	0.70			0.70		0.70
		PR	YOUT STR	RENGTH IN S	HEAR (ACI 3	18-14 17.5.3	3 or AC	CI 318-11 D.	6.3)				
Coefficient for pryout strength	k <sub>cp</sub>	-	1	1	1	1		1	2	1	2	2	2
Effective embedment depth	h <sub>ef</sub>	in. (mm)	1.20 1.94 (30) (49)		1.20 1.94 (30) (49)	1.33 1.75 (33) (44)		1.75 2.17 3.23 (44) (55) (82)		2.24 (56)			3.08 (78)
Reduction factor, pryout strength <sup>3</sup>	φ	-	(	).70	0.70	0.70		0.70	)	0.70			0.70

For **SI:** 1 inch = 25.4 mm, 1 ft-lb = 1.356 N-m, 1 psi = 0.0069 N/mm<sup>2</sup> (MPa).

N/A = Not Applicable.

<sup>1</sup>The data in this table is intended to be used with the design provisions of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable; for anchors resisting seismic load combinations the additional requirements of ACI 318-17 17.2.3 or ACI 318-11 D.3.3, as applicable shall apply.

<sup>2</sup>Installation must comply with manufacturer's published installation instructions and details.

<sup>3</sup>All values of  $\phi$  were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3, or ACI 318-11 Section 9.2. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 Section D.4.4. For reinforcement that complies with ACI 318-14 Chapter 17 or ACI 318-11 Appendix D requirements for Condition A, see ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c), as applicable, for the appropriate  $\phi$  factor when the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3, or ACI 318-11 Section 9.2 are used.

<sup>4</sup>The anchors are considered a brittle steel elements as defined by ACI 318-14 2.3 or ACI 318-11 D.1.

<sup>5</sup>Reported values for steel strength in shear are based on test results per ACI 355.2, Section 9.4 and must be used for design in lieu of the calculated results using equation 17.5.1.2b of ACI 318-14 or equation D-29 in ACI 318-11 D.6.1.2.

<sup>6</sup>Reported values for steel strength in shear are for seismic applications and based on test results in accordance with ACI 355.2, Section 9.6 and must be used for design.

<sup>7</sup>Anchors are permitted in the topside of concrete-filled steel deck assemblies in accordance with Figure 4 of this report.

<sup>8</sup>Anchors are permitted to be used in lightweight concrete in accordance with Section 4.1.12 of this report.

<sup>9</sup>Hangermate+ shear values are for threaded rod or steel inserts with and ultimate strength,  $F_u \ge 125$  ksi; threaded rod or steel inserts with an  $F_u$  less than 125 ksi are allowed provided the steel strength shear values are multiplied by the ratio of  $F_u$  (ksi) of the steel insert and 125 ksi.

## TABLE 5—TENSION AND SHEAR DESIGN INFORMATION FOR SCREW-BOLT+ AND HANGERMATE+ SCREW ANCHORS IN THE SOFFIT (THROUGH THE UNDERSIDE) OF CONCRETE-FILLED STEEL DECK ASSEMBLIES<sup>1,2,3,4,5,6,7</sup>

									No	minal	Ancho	or Size	(inch)						
Anchor Property / Setting Information	Notation	Units			/ <sub>4</sub> rmate-	F		/ <sub>4</sub> /-Bolt+		<sup>3</sup> / <sub>8</sub> rew-Bo			<sup>1</sup> / <sub>2</sub> rew-Bo	olt+	Sc	<sup>5</sup> / <sub>8</sub> rew-Bo	olt+	<sup>3</sup> / <sub>4</sub> Screw-Bolt+	
Anchor category	1, 2 or 3	-			1			1		1			1			1		1	
Head style	-	-		Thre	aded		Hex	Head	ŀ	lex Hea	ad	F	lex Hea	d	F	lex Hea	ad	Hex Head	
Threaded diameter	-	in.	1	/4	3	/ <sub>8</sub>	N	/A		N/A			N/A			N/A		N/A	
Minimum nominal embedment depth	h <sub>nom</sub>	in. (mm)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	1 <sup>5</sup> / <sub>8</sub> (41)	2 <sup>1</sup> / <sub>2</sub> (64)	2 (51)	2 <sup>1</sup> / <sub>2</sub> (64)	3 <sup>1</sup> / <sub>4</sub> (83)	2 <sup>1</sup> / <sub>2</sub> (64)	3 (76)	4 <sup>1</sup> / <sub>4</sub> (108)	3 <sup>1</sup> / <sub>4</sub> (83)	4 (102)	5 (127)	4 <sup>1</sup> / <sub>4</sub> (108)	
Effective embedment	h <sub>ef</sub>	in. (mm)	1.20 (30)	1.94 (49)	1.20 (30)	1.94 (49)	1.20 (30)	1.94 (49)	1.33 (33)	1.75 (44)	2.39 (60)	1.75 (44)	2.17 (55)	3.23 (82)	2.24 (56)	2.88 (73)	3.73 (94)	3.08 (78)	
Minimum hole depth	h₀	in. (mm)	1 <sup>3</sup> / <sub>4</sub> (44)	2 <sup>5</sup> / <sub>8</sub> (67)	1 <sup>3</sup> / <sub>4</sub> (44)	2 <sup>5</sup> / <sub>8</sub> (67)	1 <sup>3</sup> / <sub>4</sub> (44)	2 <sup>5</sup> / <sub>8</sub> (67)	2 <sup>1</sup> / <sub>8</sub> (54)	2 <sup>5</sup> / <sub>8</sub> (67)	3 <sup>3</sup> / <sub>8</sub> (86)	2 <sup>5</sup> / <sub>8</sub> (67)	3 <sup>1</sup> / <sub>8</sub> (79)	4 <sup>3</sup> / <sub>8</sub> (111)	3 <sup>3</sup> / <sub>8</sub> (86)	4 <sup>1</sup> / <sub>8</sub> (105)	5 <sup>1</sup> / <sub>8</sub> (130)	4 <sup>3</sup> / <sub>8</sub> (111)	
	See Figure	5A foi	r Scre	w-Bol	t+ and	l Figu	re 6A f	or Har	ngerm	ate+ (l	Minimu	ım 3 <sup>7</sup> /8	-inch-v	vide d	eck flu	ite)			
Minimum concrete member thickness <sup>8</sup>	h <sub>min,deck,total</sub>	in. (mm)		<sup>1</sup> / <sub>2</sub> 40)		<sup>1</sup> / <sub>2</sub> 40)		<sup>1</sup> / <sub>2</sub> 40)		5 <sup>1</sup> / <sub>2</sub> (140)			5 <sup>1</sup> / <sub>2</sub> (140)			<sup>1</sup> / <sub>2</sub> 40)	6 <sup>1</sup> / <sub>4</sub> (159)	6 <sup>1</sup> / <sub>4</sub> (159)	
Pullout strength, uncracked concrete (3,000 psi)	N <sub>p,deck,uncr</sub>	lb (kN)		430 .4)		2,555 (11.4)	1,430 (6.4)	2,555 (11.4)			3,235 (14.4)	2,600 (11.6)			2,610 (11.6)		6,195 (27.6)	6,085 (27.1)	
Pullout strength, cracked concrete (3,000 psi)	N <sub>p,deck,cr</sub>	lb (kN)	-	15 .7)	615 (2.7)	1,115 (5.0)	615 (2.7)	1,115 (5.0)	1,290 (5.1)	1,880 (8.4)	2,290 (10.2)	1,230 (5.5)	2,330 (10.4)	4,030 (17.9)		3,340 (14.9)	4,945 (22.0)	3,835 (17.1)	
Pullout strength, seismic (3,000 psi)	N <sub>p,deck,eq</sub>	lb (kN)		90 .3)	290 (1.3)	920 (4.1)	290 (1.3)	920 (4.1)	890 (4.0)	1,570 (7.0)	2,015 (9.0)	1,230 (5.5)	2,330 (10.4)	4,030 (17.9)	990 (4.4)	1,730 (7.7)	2,415 (10.8)	3,410 (15.2)	
Reduction factor, pullout strength <sup>9</sup>	$\phi$	-		0.	65		0.	65		0.65			0.65			0.65		0.65	
Steel strength in shear	V <sub>sa,deck</sub>	lb (kN)		485 .6)		'40 ?.2)	1,155 (5.1)	2,595 (11.6)		2,540 (11.3)		2,435 (10.8)	2,435 (10.8)	5,845 (26.0)			6,325 (28.1)	5,175 (23.0)	
Steel strength in shear, seismic	V <sub>sa,deck.eq</sub>	lb (kN)		1,040 (4.6)				960 2165 (4.3) (9.6)		1,775 (7.9)	1,950 (8.7)	2,250 (10.0)	1,950 (8.7)	2,095 (9.3)	4,675 (20.8)	2,120 (9.4)	2,325 (10.3)	5,060 (22.5)	4,140 (18.4)
Reduction factor, steel strength in shear <sup>9</sup>	φ	-		0.	60		0.	60		0.60			0.60			0.60		0.60	
	See Figure	e 5B fo	or Scre	ew-Bo	lt+ an	d Figu	ıre 6B	for Ha	ngern	nate+ (	Minim	um 1³/,	₄-inch-	wide d	leck flu	ute)			
Minimum concrete member thickness <sup>8</sup>	h <sub>min,deck,total</sub>	in. (mm)		4 02)		4 02)		4 02)		4 (102)		4 (102)	N	/A		N/A		N/A	
Pullout strength, uncracked concrete (3,000 psi)	N <sub>p,deck,uncr</sub>	lb (kN)		760 .8)	1,760 (7.8)	2,075 (9.2)	1,760 (7.8)	2,075 (9.2)	1,440 (6.4)	2,135 (9.5)	3,190 (14.2)	1,720 (7.6)							
Pullout strength, cracked concrete (3,000 psi)	N <sub>p,deck,cr</sub>	lb (kN)		60 .4)	770 (3.4)	910 (4.0)	760 (3.4)	910 (4.0)	815 (3.6)	1,510 (6.7)	2,260 (10.0)	1280 (5.7)	N	/A		N/A		N/A	
Pullout strength, seismic (3,000 psi)	N <sub>p,deck,eq</sub>	lb (kN)		55 .6)	635 (2.8)	750 (3.3)	355 (1.6)	750 (3.3)	565 (2.5)	1,260 (5.6)	1,985 (8.8)	1280 (5.7)							
Reduction factor, pullout strength <sup>9</sup>	φ	-		0.	65		0.	65		0.65	·	0.65							
Steel strength in shear	V <sub>sa,deck</sub>	lb (kN)		680 .5)	2,1 (9	80 .7)	1,880 (8.4)	2,315 (10.3)		2,115 (9.4)	2,820 (12.5)	2,095 (9.3)							
Steel strength in shear, seismic	V <sub>sa,deck.eq</sub>	lb (kN)		175 .2)		960 .7)	1,565 (7.0)	1,930 (8.6)	1,475 (6.6)	1,620 (5.6)	1,965 (8.7)	1,675 (7.5)	N	/A		N/A		N/A	
Reduction factor, steel strength in shear <sup>9</sup>	$\phi$	-		0.	60		0.	60		0.60		0.60							

For **SI:** 1 inch = 25.4 mm, 1 ft-lb = 1.356 N-m, 1 psi = 0.0069 N/mm<sup>2</sup> (MPa).

N/A = Not Applicable.

<sup>1</sup>Installation must comply with manufacturer's published installation instructions and details.

<sup>2</sup>Values for  $N_{p,deck,and}$   $N_{p,deck,cr}$  are for sand-lightweight concrete ( $f'_{c,min}$  = 3,000 psi) and additional lightweight concrete reduction factors need not be applied. In addition, evaluation for the concrete breakout capacity in accordance with ACI 318-14 17.4.2 or ACI 318 D.5.2, as applicable, is not required for anchors installed in the deck soffit (through underside).

<sup>3</sup>Values for  $N_{p,deck,eq}$  are applicable for seismic loading; see Section 4.1.8.2 of this report.

<sup>4</sup>For the calculation of  $N_{pr}$ , see Section 4.1.4 of this report; for all design cases  $\Psi_{c,P} = 1.0$ . The characteristic pullout strength for concrete compressive strengths greater than 3,000 psi for  $^{1}/_{4}$ -inch-diameter anchors may be increased by multiplying the value in the table by  $(f_{c}^{r}/3,000)^{0.3}$  for psi or  $(f_{c}^{r}/17.2)^{0.3}$  for MPa. The characteristic pullout strength for concrete compressive strengths greater than 3,000 psi for  $^{3}/_{8}$ -inch-diameter anchors may be increased by multiplying the value in the table by  $(f_{c}^{r}/3,000)^{0.3}$  for MPa. The characteristic pullout strength for concrete compressive strengths greater than 3,000 psi for  $^{3}/_{8}$ -inch-diameter anchors may be increased by multiplying the value in the table by  $(f_{c}^{r}/3,000)^{0.5}$  for psi or  $(f_{c}^{r}/17.2)^{0.5}$  for MPa.

<sup>5</sup>Shear loads for anchors installed through steel deck into concrete may be applied in any direction.

<sup>6</sup>Values of  $V_{sa,deck}$  and  $V_{sa,deck,eq}$  are for sand-lightweight concrete and additional lightweight concrete reduction factors need not be applied. In addition, evaluation for the concrete breakout capacity in accordance with ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, and the pryout capacity in accordance with ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, and the pryout capacity in accordance with ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable, are not required for anchors installed in the soffit (through underside). <sup>7</sup>Hangermate+ shear values are for threaded rod or steel inserts with and ultimate strength,  $F_u \ge 125$  ksi; threaded rod or steel inserts with an  $F_u$  less than 125 ksi are allowed provided the steel strength shear values are multiplied by the ratio of  $F_u$  (ksi) of the steel insert and 125 ksi.

<sup>9</sup>The minimum concrete member thickness,  $h_{min,deck,totah}$  is the minimum overall thickness of the concrete-filled steel deck (depth and topping thickness). <sup>9</sup>All values of  $\phi$  were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318 Section 9.2. If the load combinations of ACI 318 Appendix C are used, then the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4 (ACI 318-08).

Anchor	Nominal Anchor Diameter (in.)	Nominal Embedment Depth (in.)	Effective Embedment (in.)	Allowable Tension Load (lbs)
	1/4	1 <sup>5</sup> / <sub>8</sub>	1.20	780
	/4	2 <sup>1</sup> / <sub>2</sub>	1.94	1,425
		2	1.33	1,010
	<sup>3</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>2</sub>	1.75	1,220
		3 <sup>1</sup> / <sub>4</sub>	2.39	1,950
Corow Dolt		2 <sup>1</sup> / <sub>2</sub>	1.75	1,525
Screw-Bolt+	<sup>1</sup> / <sub>2</sub>	3	2.17	1,685
		4 <sup>1</sup> / <sub>4</sub>	3.23	3,060
		3 <sup>1</sup> / <sub>4</sub>	2.24	2,210
	<sup>5</sup> /8	4	2.88	2,575
		5	3.73	3,795
	<sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>	3.08	3,205
	1/4	1 <sup>5</sup> / <sub>8</sub>	1.20	780
Llangarmata	/4	2 <sup>1</sup> / <sub>2</sub>	1.94	1,425
Hangermate+	<sup>3</sup> / <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	1.20	780
	/8	2 <sup>1</sup> / <sub>2</sub>	1.94	1,425

TABLE 6—EXAMPLE ALLOWABLE STRESS DESIGN VALUES FOR ILLUSTRATIVE PURPOSES<sup>1,2,3,4,5,6,7,8,9</sup>

For **SI:** 1 inch = 25.4 mm; 1 lbf = 0.0044 kN.

Illustrative Allowable Stress Design Values in Table 7 are applicable only when the following design assumptions are followed:

<sup>1</sup>Single anchor with static tension load only.

<sup>2</sup>Concrete determined to remain uncracked for the life of the anchorage.

<sup>3</sup>Load combinations from ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2, as applicable, (no seismic loading).

 $^{4}_{2}$ 30% dead load and 70% live load, controlling load combination: 1.2D + 1.6L.

<sup>5</sup>Calculated of weighted average for  $\alpha = 1.2(0.3) + 1.6(0.7) = 1.48$ .

 $\int_{-6}^{6} f'_c = 2,500$  psi (normal weight concrete).

 $\int_{8}^{7} C_{a1} = C_{a2} \ge C_{ac}.$ 

 $^{8}h \geq h_{min}$ 

<sup>9</sup>Values are for Condition B; supplementary reinforcement in accordance with ACI 318-14 17.3.3 or ACI 318-11 D.4.3 is not provided, as applicable.

Calculation in accordance with ACI 318-14 Chapter 17 or ACI 318-11 Appendix D and this report:	Code Ref.	Report Ref
Step 1. Calculate steel strength of a single anchor in tension:	D.5.1.2 (318-11)	Table 3
$\phi N_{sa} = (0.65)(20,475) = 13,309 \ lbs.$	17.4.1.2 (318-14)	§4.1.2
Step 2. Calculate concrete breakout strength of a single anchor in tension:	D.5.2.1 (318-11)	Table 3
$\phi N_{cb} = \phi \frac{A_{Nc}}{A_{Nc0}} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b$	17.4.2.1 (318-14)	§4.1.3
$N_b = k_c \lambda_a \sqrt{f'_c} (h_{ef})^{1.5}$	D.5.2.2 (318-11) 17.4.2.2 (318-14)	Table 3
$N_b = (24)(1.0)\sqrt{2,500}(2.17)^{1.5} = 3,836 \ lbs.$		
$\phi N_{cb} = (0.65) \frac{(42.4)}{(42.4)} (1.0) (1.0) (1.0) (3,836) = 2,493 \ lbs.$		
Step 3. Calculate pullout strength:		
$\phi N_{pn} = \phi N_{p,uncr} \psi_{c,P}$	D.5.3.2 (318-11) 17.4.3.2 (318-14)	Table 3 §4.1.4
$\phi N_{pn}$ = n/a (pullout strength does not control per reported design values)	17.4.0.2 (010 14)	34.1.4
Step 4. Determine controlling resistance strength in tension:	D.4.1.1 (318-11)	
$\boldsymbol{\phi} \boldsymbol{N}_{\boldsymbol{n}} = \min \left  \boldsymbol{\phi} \boldsymbol{N}_{sa}, \boldsymbol{\phi} \boldsymbol{N}_{cb}, \boldsymbol{\phi} \boldsymbol{N}_{pn} \right  = \left  \boldsymbol{\phi} \boldsymbol{N}_{cb} \right  = 2,493 \ lbs.$	17.3.1.1 (318-14)	
Step 5. Calculate allowable stress design conversion factor for loading condition:	9.2 (ACI 318-11)	
Controlling load combination: 1.2D + 1.6L	5.2 (ACI 318-14)	
$\alpha = 1.2(30\%) + 1.6(70\%) = 1.48$		
Step 6. Calculate allowable stress design value		
$T_{allowable,ASD} = \frac{\phi N_n}{\alpha} = \frac{2,493}{1.48} = 1,685 \ lbs.$		§4.2

FIGURE 7—EXAMPLE STRENGTH DESIGN CALCULATION INCLUDING ASD CONVERSION, FOR ILLUSTRATIVE PURPOSES



## **ICC-ES Evaluation Report**

## **ESR-3889 LABC and LARC Supplement**

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00—METALS Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

DEWALT

**EVALUATION SUBJECT:** 

SCREW-BOLT+™ SCREW ANCHORS AND HANGERMATE<sup>®</sup>+ ROD HANGER SCREW ANCHORS IN CRACKED AND UNCRACKED CONCRETE (DEWALT)

#### 1.0 REPORT PURPOSE AND SCOPE

Purpose:

The purpose of this evaluation report supplement is to indicate that Screw-Bolt+ Screw Anchors and Hangermate+ Rod Hanger Screw Anchors in cracked and uncracked concrete, described in ICC-ES master evaluation report <u>ESR-3889</u>, have also been evaluated for compliance with the codes noted below as adopted by Los Angeles Department of Building and Safety (LADBS).

#### Applicable code editions:

- 2017 City of Los Angeles Building Code (LABC)
- 2017 City of Los Angeles Residential Code (LARC)

#### 2.0 CONCLUSIONS

The Screw-Bolt+ Screw Anchors and Hangermate+ Rod Hanger Screw Anchors in cracked and uncracked concrete, described in Sections 2.0 through 7.0 of the master evaluation report <u>ESR-3889</u>, comply with LABC Chapter 19, and LARC, and are subjected to the conditions of use described in this report.

#### 3.0 CONDITIONS OF USE

The Screw-Bolt+ and Hangermate+ anchors described in this evaluation report must comply with all of the following conditions:

- All applicable sections in the master evaluation report ESR-3889.
- The design, installation, conditions of use and labeling of the anchors are in accordance with the 2015 International Building Code<sup>®</sup> (2015 IBC) provisions noted in the master evaluation report ESR-3889.
- The design, installation and inspection are in accordance with additional requirements of LABC Chapters 16 and 17, as applicable.
- Under the LARC, an engineered design in accordance with LARC Section R301.1.3 must be submitted.
- The allowable and strength design values listed in the master evaluation report and tables are for the connection of the anchors to the concrete. The connection between the anchors and the connected members shall be checked for capacity (which may govern).

This supplement expires concurrently with the master report, reissued November 2018.

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00—METALS Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

DEWALT

**EVALUATION SUBJECT:** 

SCREW-BOLT+™ SCREW ANCHORS AND HANGERMATE<sup>®</sup>+ ROD HANGER SCREW ANCHORS IN CRACKED AND UNCRACKED CONCRETE (DEWALT)

#### 1.0 REPORT PURPOSE AND SCOPE

#### Purpose:

The purpose of this evaluation report supplement is to indicate that Screw-Bolt+ Screw Anchors and Hangermate+ Rod Hanger Screw Anchors in Cracked and Uncracked Concrete, recognized in ICC-ES master evaluation report ESR-3889, have also been evaluated for compliance with the codes noted below:

#### Compliance with the following codes:

- 2017 Florida Building Code—Building
- 2017 Florida Building Code—Residential

#### 2.0 CONCLUSIONS

The Screw-Bolt+ Screw Anchors and Hangermate+ Rod Hanger Screw Anchors in Cracked and Uncracked Concrete described in Sections 2.0 through 7.0 of the master evaluation report ESR-3889 comply with the *Florida Building Code*—*Building* and the *Florida Building Code*—*Residential*, provided the design and installation are in accordance with the 2015 International Building Code<sup>®</sup> provisions noted in the master evaluation report.

Use of the Screw-Bolt+ Screw Anchors and Hangermate+ Rod Hanger Screw Anchors in cracked and uncracked concrete as described in the master evaluation report for compliance with the High-Velocity Hurricane Zone provisions of the *Florida Building Code—Building Code—Building Code—Building Code—Building Code—Residential* has not been evaluated, and is outside the scope of this supplement.

For products falling under Florida Rule 9N-3, verification that the report holder's quality-assurance program is audited by a quality-assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official, when the report holder does not possess an approval by the Commission).

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