## 

PIONEERING REUSABILITY AND CONVENIENCE IN THE SCREW ANCHOR MARKET<br>KWIK HUS Reusability System

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KWIK HUS Reusability System

## lity

With the Hilti Reusability Gauge (HRG), Hilti allows and provides guidance for reusing its KWIK HUS screw anchor.

Screw anchor holding values are influenced by the ability of the screw's threads to bear against the concrete. Reusing an anchor will overtime reduce the diameter of it's threads, thereby reducing the anchor's holding values. Hilti publishes load values for both single-use and reused anchors - and has developed a matcheddiameter "go/no-go" HRG gauge to verify the anchor is suitable for reuse.

With up to 20 reuses, the cost per fastening point can be significantly reduced, improving profitability and productivity.

This makes the KWIK HUS the first screw anchor that allows the installer to... Drill. Drive. Done... Reuse.

## Productivity

- Removable and reusable, reducing the amount of anchors needed per project and cost per fastening point
- More than $50 \%$ installation time savings over coil and stud anchors
- Higher number of reuses allowed compared to coil anchors
- No additional coil component needed to purchase


## Reliability

- Reusability gauge quickly identifies if the anchor is still within its useful life
- Published load capacity listings for reused anchors provide guidance to installers and engineers


Great for temporary bracing...

... and temporary railings


In the example below, using a 1/2" screw anchor after 20 uses drops the price per fastening point to just $\$ 0.08$. Coupled with the installation time savings of more than $50 \%$ when inserting a screw anchor versus a coil anchor, installing KWIK HUS screws with the HRG can lead to thousands of dollars in savings per project. Note: Number of reuses is dependent upon the anchor diameter and the concrete compressive strength.


## SCREW ANCHOR KWIK HUS

## Applications and advantages

- Attaching formwork and tilt-up braces, sill plates, perimeter walls
- Racking and shelving
- Attaching ledgers
- For use with standard ANSI-tolerance drill bit; no special tolerance drill bits are required
- Tested and evaluated according to AC193 for uncracked concrete and AC106 for grout-filled CMU blocks

|  |  |
| :---: | :---: |
| Technical data |  |
| Approvals / Test reports | Nuclear (NQA-1) ${ }^{1}$ |
| Environmental conditions | Indoor, dry conditions |
| Head configuration | Hex head |
| Installation direction | All |
| Material, corrosion | Steel, zinc-plated to a min. thickness of $8 \mu \mathrm{~m}$ |
| Type of fixing | Through-fastening |

## Screw anchor KWIK HUS order information

| Order Designation | Drill bit diameter | Anchor length | Box only |  | Master carton 1x |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sales pack quantity | Item number | Sales pack quantity | Item number |
| Screw anchor KH 1/4" $\times 2-5 / 8^{\prime \prime}$ | 1/4 in | 2-5/8 in | 100 pc | 2309298 | 800 pc | 3704533 |
| Screw anchor KH 3/8" $\times$ 2-1/8" | $3 / 8$ in | 2-1/8 in | 50 pc | 434436 | 450 pc | 3465007 |
| Screw anchor KH 3/8 x 3" | $3 / 8$ in | 3 in | 50 pc | 434437 | 300 pc | 3465008 |
| Screw anchor KH 3/8" $\times$ 3-1/2" | $3 / 8$ in | 3-1/2 in | 50 pc | 434438 | 300 pc | 3465009 |
| Screw anchor KH 3/8" $\times 4$ " | $3 / 8$ in | 4 in | 50 pc | 434439 | 300 pc | 3465010 |
| Screw anchor KH 3/8" $\times$ 5" | $3 / 8$ in | 5 in | 30 pc | 434440 | 270 pc | 3465011 |
| Screw anchor KH 1/2" x 3" | $1 / 2$ in | 3 in | 30 pc | 434441 | 180 pc | 3465012 |
| Screw anchor KH 1/2" x 3-1/2" | $1 / 2$ in | $3-1 / 2$ in | 25 pc | 434442 | 150 pc | 3465013 |
| Screw anchor KH 1/2" x 4" | $1 / 2$ in | 4 in | 25 pc | 434443 | 150 pc | 3465014 |
| Screw anchor KH 1/2" x 4-1/2" | $1 / 2$ in | 4-1/2 in | 25 pc | 434444 | 150 pc | 3465015 |
| Screw anchor KH 1/2" x 5" | $1 / 2$ in | 5 in | 25 pc | 434445 | 150 pc | 3465016 |
| Screw anchor KH 1/2" x 6" | $1 / 2$ in | 6 in | 25 pc | 434446 | 150 pc | 3465017 |
| Screw anchor KH 5/8" $\times$ 4" | $5 / 8$ in | 4 in | 15 pc | 434447 | 90 pc | 3465018 |
| Screw anchor KH 5/8" $\times$ 5-1/2" | $5 / 8$ in | 5-1/2 in | 15 pc | 434448 | 90 pc | 3465019 |
| Screw anchor KH 5/8" $\times$ 6-1/2" | $5 / 8$ in | 6-1/2 in | 15 pc | 434449 | 45 pc | 3465020 |
| Screw anchor KH 3/4" x 4-1/2" | $3 / 4$ in | 4-1/2 in | 10 pc | 434450 | 60 pc | 3465021 |
| Screw anchor KH 3/4" x 5-1/2" | $3 / 4$ in | 5-1/2 in | 10 pc | 434451 | 30 pc | 3465022 |
| Screw anchor KH 3/4" x 7" | $3 / 4$ in | 7 in | 10 pc | 434452 | 40 pc | 3465023 |
| Screw anchor KH 3/4" x 9" | $3 / 4$ in | 9 in | 10 pc | 434453 | 40 pc | 3465024 |

HRG - KWIK HUS anchor reusability gauge

| Order Designation | Diameter | Sales pack quantity | Item number |
| :---: | :---: | :---: | :---: |
| Hilti reusability gauge HRG 1/4" | 1/4 in | $1 \mathrm{pc}^{1}$ | 2309298 |
| Hilti reusability gauge HRG 3/8" | $3 / 8$ in | 1 pc | 2122554 |
| Hilti reusability gauge HRG 1/2" | 1/2 in | 1 pc | 2122555 |
| Hilti reusability gauge HRG 5/8" | $5 / 8$ in | 1 pc | 2122556 |
| Hilti reusability gauge HRG 3/4" | $3 / 4$ in | 1 pc | 2122557 |

The Hilti Reusability Gauge (HRG) indicates to the installer if the anchor has exceeded its useful life prior to installation.

## Hilti Reusability Solution



## PRODUCT DESCRIPTION

The Hilti Reusable Gauge (HRG) is a zinc-plated hollow steel tube used with the Hilti KWIK HUS (KH) screw anchor for reuse applications (e.g. concrete formwork, tilt-up bracing, temporary railings and opening coverings). Each KH diameter has a corresponding HRG that can be attached to a Hilti impact wrench. A KH can be installed, used, and removed multiple times until the HRG indicates whether the threads on the anchor have been worn beyond their useful life. The concept is simple: if the KH does not pass through the length of the HRG, it can continue to be used with the "reused" published loads in this document.

## DESCRIPTION OF TECHNICAL DATA

## Testing and Product Evaluation

Hilti KWIK HUS screw anchors were continually reused in concrete until the screw threads met the lifetime limits as indicated by the HRG. The worn down KH screws were then tested in tension and shear and nominal capacities were determined based on ICC Evaluation Services (ICC-ES) Acceptance Criteria for Post-installed Mechanical Anchors in Concrete Elements (AC193), which incorporates the requirements of ACl 355.2 .

## Anchor Design Codes

- United States — Design strength calculated using ACI 318 Chapter 17.
- Canada - Factored resistance calculated using CSA A23.3 Annex D.

Design of KWIK HUS Mechanical Anchor System with Hilti Reusable Gauge

## Determination of Nominal Strengths (ACI) and Nominal Resistances (CSA)

The nominal strength (ACI), or nominal resistance (CSA), determined through testing according to AC193 / ACI 355.2 or calculation through ACI 318 Ch. 17 / CSA A23.3 Annex D is multiplied by strength modification factors, resulting in a design strength (ACI), or factored resistance (CSA), for the KH anchor. Design strengths (factored resistances) are provided in Table 3 of this document for KH anchors worn to the limits of the HRG inner diameters.

ACI:
$\mathrm{N}_{\mathrm{n}}=$ Nominal strength in tension (lesser of concrete, pullout, or steel strength)
$\mathrm{V}_{\mathrm{n}}=$ Nominal strength in shear (lesser of pryout or steel strength)
$\phi=$ Strength reduction factor
$\phi N_{n}=$ Design strength in tension
$\phi V_{n}=$ Design strength in shear
CSA:
$N_{n}=$ Nominal strength in tension (lesser of concrete, pullout, or steel strength)
$\mathrm{V}_{\mathrm{n}}=$ Nominal strength in shear (lesser of pryout or steel strength)
$\phi=$ Material resistance factor
R = Resistance modification factor
$N_{r}=$ Factored resistance in tension $=\phi N_{n} R$
$V_{r}=$ Factored resistance in shear $=\phi V_{n} R$

## Interaction of Tension and Shear

Where anchors are loaded simultaneously in tension and shear, interaction must be considered. Applicable ACI 318 Ch. 17 and CSA A23.3 Annex D anchorage interaction equations are given below.

ACI: $\frac{N_{\text {ua }}}{\phi N_{\mathrm{n}}}+\frac{\mathrm{V}_{\mathrm{ua}}}{\phi \mathrm{V}_{\mathrm{n}}} \leq 1.2$
where:
$\mathrm{N}_{\mathrm{ua}}=$ Required strength in tension based on factored load combinations of ACI 318-19 Chapter 5
$\mathrm{V}_{\mathrm{ua}}=$ Required strength in shear based on factored load combinations of ACl 318-19 Chapter 5
$\operatorname{CSA}: \frac{N_{f}}{N_{r}}+\frac{V_{f}}{V_{r}} \leq 1.2$
where:
$N_{f}=$ Required strength in tension based on factored load combinations of CSA A23.3-19 Chapter 8
$V_{f}=$ Required strength in shear based on factored load combinations of CSA A23.3-19 Chapter 8
The full tensile strength can be permitted if:
ACI: $\frac{V_{\text {ua }}}{\phi V_{n}} \leq 0.2 \quad$ CSA: $\frac{V_{f}}{V_{r}} \leq 0.2$

The full shear strength can be permitted if:
ACI: $\frac{N_{u a}}{\phi N_{n}} \leq 0.2 \quad$ CSA: $\frac{N_{f}}{N_{r}} \leq 0.2$

## Allowable Stress Design

The design strength (factored resistance) values in Tables 2 and 3 can be converted to an Allowable Stress Design (ASD) value as follows:
$N_{\text {ASD }}=\frac{\phi N_{n}}{\alpha_{A S D}}$
$V_{A S D}=\frac{\phi V_{n}}{\alpha_{\text {ASD }}}$
where
$\alpha_{\text {ASD }}=$ Conversion factor calculated as a weighted average of the LRFD load factors normalized by the ASD load factors for the controlling load combination. Guidance for calculation of $\propto_{\text {ASD }}$ is given at:
http://www.icc-es.org/News/Notices/ES/SD-ASD Letter.pdf.
Some examples of $\alpha_{\text {ASD }}$ for specific cases are provided below:

- Pure wind load: $\propto_{\text {ASD,w }}=1.67$
- Pure live load: $\alpha_{\text {Asd,L }}=1.6$
- Pure dead load: $\propto_{\text {ASD,D }}=1.4$
- 50\% dead load, $50 \%$ live load: $\propto_{A S D, D L}=1.4$

C-ITri

Table 1 - Reused KWIK HUS installation parameters for temporary applications with the Hilti HRG ${ }^{1}$

| Characteristic | Symbol | Units | Nominal anchor diameter (in.) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/4 |  | 3/8 |  |  | 1/2 |  |  | 5/8 |  | 3/4 |  |
| Nominal bit diameter | $\mathrm{d}_{\text {bit }}$ | in. | 1/4 |  | 3/8 |  |  | 1/2 |  |  | 5/8 |  | 3/4 |  |
| Fixture hole diameter | $\mathrm{d}_{\mathrm{h}}$ | $\begin{aligned} & \text { in. } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{array}{r} \hline 3 / 8 \\ (10) \\ \hline \end{array}$ |  | $\begin{array}{r} \hline 1 / 2 \\ (13) \\ \hline \end{array}$ |  |  | $\begin{array}{r} \hline 5 / 8 \\ (16) \\ \hline \end{array}$ |  |  | $\begin{array}{r} \hline 3 / 4 \\ (19) \\ \hline \end{array}$ |  | $\begin{array}{r} \hline 7 / 8 \\ (22) \\ \hline \end{array}$ |  |
| Installation torque ${ }^{2}$ | $\mathrm{T}_{\text {inst }}$ | $\mathrm{ft}-\mathrm{lb}$ <br> (Nm) | $\begin{gathered} 10 \\ (14) \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 40 \\ (54) \\ \hline \end{gathered}$ |  |  | $\begin{gathered} 45 \\ (61) \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \hline 85 \\ (115) \end{gathered}$ |  | $\begin{gathered} \hline 95 \\ (129) \end{gathered}$ |  |
| Maximum impact wrench torque rating with $\mathrm{f}_{\mathrm{c}}{ }_{\mathrm{c}}>3,000 \mathrm{psi}{ }^{3}$ | $\mathrm{T}_{\text {impact }}$ | $\begin{aligned} & \mathrm{ft}-\mathrm{lb} \\ & (\mathrm{Nm}) \end{aligned}$ | $\begin{gathered} \hline 66 \\ (89) \\ \hline \end{gathered}$ |  | $\begin{gathered} 122 \\ (165) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 148 \\ (201) \\ \hline \end{gathered}$ |  | $\begin{gathered} 122 \\ (165) \\ \hline \end{gathered}$ | $\begin{gathered} 148 \\ (201) \\ \hline \end{gathered}$ |  | $\begin{aligned} & \hline 330 \\ & (447) \\ & \hline \end{aligned}$ |  | $\begin{gathered} 330 \\ (447) \\ \hline \end{gathered}$ |  |
| Maximum impact wrench torque rating with $\mathrm{f}_{\mathrm{c}}{ }^{\circ}<3,000 \mathrm{psi}^{3}$ | $\mathrm{T}_{\text {impact }}$ | $\begin{aligned} & \mathrm{ft}-\mathrm{lb} \\ & (\mathrm{Nm}) \end{aligned}$ | $\begin{gathered} \hline 44 \\ (60) \\ \hline \end{gathered}$ |  | $\begin{gathered} 44 \\ (60) \\ \hline \end{gathered}$ | $\begin{gathered} 100 \\ (136) \\ \hline \end{gathered}$ |  | $\begin{gathered} 100 \\ (136) \\ \hline \end{gathered}$ |  |  | $\begin{gathered} 148 \\ (201) \\ \hline \end{gathered}$ | $\begin{gathered} 330 \\ (447) \\ \hline \end{gathered}$ | $\begin{gathered} 330 \\ (447) \\ \hline \end{gathered}$ |  |
| Nominal embedment | $\mathrm{h}_{\text {nom }}$ | in. (mm) | $\begin{gathered} 1-1 / 8 \\ (83) \\ \hline \end{gathered}$ | $\begin{aligned} & 1-5 / 8 \\ & (127) \\ & \hline \end{aligned}$ | $1-5 / 8$ <br> (41) | 2-1/2 <br> (64) | $\begin{gathered} 3-1 / 4 \\ (83) \\ \hline \end{gathered}$ | $\begin{gathered} 2-1 / 4 \\ (57) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 \\ (76) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 4-1 / 4 \\ & (108) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 3-1 / 4 \\ (83) \\ \hline \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} \hline 4 \\ (102) \\ \hline \end{gathered}$ | $\begin{aligned} & 6-1 / 4 \\ & (159) \end{aligned}$ |
| Effective embedment | $\mathrm{h}_{\text {ef }}$ | in. (mm) | $\begin{aligned} & 0.75 \\ & (19) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.18 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.11 \\ & (28) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.86 \\ & (47) \\ & \hline \end{aligned}$ | $\begin{array}{r} 2.20 \\ (56) \\ \hline \end{array}$ | $\begin{aligned} & 1.52 \\ & (39) \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline 2.16 \\ (55) \\ \hline \end{array}$ | $\begin{aligned} & \hline 3.22 \\ & (82) \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline 2.39 \\ (61) \\ \hline \end{array}$ | $\begin{gathered} 3.88 \\ (99) \\ \hline \end{gathered}$ | $\begin{array}{r} \hline 2.92 \\ (74) \\ \hline \end{array}$ | $\begin{aligned} & 4.84 \\ & (123) \\ & \hline \end{aligned}$ |
| Minimum hole depth | h。 | $\begin{aligned} & \text { in. } \\ & \text { (mm) } \end{aligned}$ | $\begin{gathered} 1-3 / 8 \\ (35) \\ \hline \end{gathered}$ | $\begin{gathered} 1-7 / 8 \\ (48) \\ \hline \end{gathered}$ | $\begin{gathered} 1-5 / 8 \\ (41) \\ \hline \end{gathered}$ | $\begin{gathered} 2-3 / 4 \\ (70) \\ \hline \end{gathered}$ | $\begin{gathered} 3-1 / 2 \\ (89) \\ \hline \end{gathered}$ | $\begin{gathered} 2-5 / 8 \\ (67) \end{gathered}$ | $\begin{gathered} 3-3 / 8 \\ (86) \\ \hline \end{gathered}$ | $\begin{gathered} 4-5 / 8 \\ (117) \\ \hline \end{gathered}$ | $\begin{gathered} 3-5 / 8 \\ (92) \\ \hline \end{gathered}$ | $\begin{aligned} & 5-3 / 8 \\ & (137) \\ & \hline \end{aligned}$ | $\begin{gathered} 4-3 / 8 \\ (111) \\ \hline \end{gathered}$ | $\begin{aligned} & 6-5 / 8 \\ & (168) \\ & \hline \end{aligned}$ |
| Minimum edge distance in tension and in direction of shear loading | $\mathrm{C}_{\mathrm{a} 1}$ | $\begin{aligned} & \text { in. } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{gathered} 1-1 / 2 \\ (38) \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 3-3 / 8 \\ (85) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 5-1 / 4 \\ & (133) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 6 \\ (154) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 4-1 / 8 \\ & (106) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5-5 / 8 \\ & (143) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 8-3 / 8 \\ & (214) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6-3 / 8 \\ & (162) \\ & \hline \end{aligned}$ | $\begin{gathered} 10 \\ (253) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 10 \\ (253) \\ \hline \end{gathered}$ | $\begin{array}{\|c} \hline 12-1 / 8 \\ (308) \\ \hline \end{array}$ |
| Minimum edge distance parallel to shear load direction | $\mathrm{C}_{\mathrm{a} 2}$ | $\begin{aligned} & \text { in. } \\ & (\mathrm{mm}) \end{aligned}$ | $2$(51) |  | $\begin{gathered} 5 \\ (128) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7-7 / 8 \\ & (200) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 9-1 / 8 \\ & (231) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6-1 / 4 \\ & (159) \\ & \hline \end{aligned}$ | $\begin{aligned} & 8-1 / 2 \\ & (215) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 12-5 / 8 \\ (321) \\ \hline \end{gathered}$ | $\begin{aligned} & 9-1 / 2 \\ & (243) \end{aligned}$ | $\begin{gathered} 15 \\ (380) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (379) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 18-1 / 4 \\ (463) \\ \hline \end{gathered}$ |
| Minimum spacing | $\mathrm{S}_{\text {min }}$ | $\begin{aligned} & \text { in. } \\ & \text { (mm) } \end{aligned}$ | $\begin{gathered} 3 \\ (76) \\ \hline \end{gathered}$ |  | $\begin{aligned} & 4-7 / 8 \\ & (124) \\ & \hline \end{aligned}$ | $\begin{aligned} & 7-1 / 2 \\ & (191) \end{aligned}$ | $\begin{aligned} & 9-3 / 4 \\ & (248) \end{aligned}$ | $\begin{aligned} & 6-3 / 4 \\ & (171) \end{aligned}$ | $\begin{gathered} 9 \\ (229) \end{gathered}$ | $\begin{gathered} 12-3 / 4 \\ (324) \end{gathered}$ | $\begin{aligned} & 9-3 / 4 \\ & (248) \end{aligned}$ | $\begin{gathered} 15 \\ (381) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (305) \\ \hline \end{gathered}$ | $\begin{gathered} 18-3 / 4 \\ (476) \end{gathered}$ |
| Minimum concrete thickness | $\mathrm{h}_{\text {min }}$ | $\begin{gathered} \hline \text { in. } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \hline 3-1 / 4 \\ (83) \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 3-1 / 4 \\ (83) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 4 \\ (102) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 4-7 / 8 \\ & (124) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 3-3 / 4 \\ (95) \\ \hline \end{gathered}$ | $\begin{gathered} 4-3 / 4 \\ (121) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 6-3 / 4 \\ & (171) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 5 \\ (127) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (178) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (152) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 8-1 / 8 \\ & (206) \\ & \hline \end{aligned}$ |
| Wrench size | - | $\begin{aligned} & \text { in. } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \hline 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ |  |  | $\begin{array}{r} \hline 3 / 4 \\ (19) \\ \hline \end{array}$ |  |  | $\begin{gathered} 15 / 16 \\ (24) \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 1-1 / 8 \\ (29) \\ \hline \end{gathered}$ |  |

1 See Figure 1 for installation parameters intended for re-used KH measured with HRG.
$2 \mathrm{~T}_{\text {inst }}$ applies to installations using a calibrated torque wrench.
3 Torque ratings of Hilti impact tools. Because of variability in measurement procedures, the published torque of an impact tool may not correlate properly with the above setting torques. Over-torqueing can damage the anchor and/or reduce its holding capacity.


Figure 1 - Illustration of KWIK HUS installation parameters for reuse.

Table 2 - Single-use Hilti KWIK HUS design strength (factored resistance) in uncracked concrete ${ }^{1,2}$ IMPORTANT: these values are higher as compared to a reused anchor

| Nominal anchor diameter in. | Nominal embedment in. (mm) |  | $\begin{gathered} \mathbf{f}^{\prime}=2000 \mathrm{psi} \\ (13.7 \mathrm{MPa}) \end{gathered}$ |  |  |  |  |  | $\begin{gathered} \mathbf{f}^{\prime}=4000 \mathrm{psi} \\ (27.5 \mathrm{MPa}) \end{gathered}$ |  |  |  |  |  | $\begin{gathered} \mathrm{f}^{\prime}=6000 \mathrm{psi} \\ (41.2 \mathrm{MPa}) \end{gathered}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tension $\phi N_{n}$ or $N_{r}$ <br> lb (kN) |  | Shear $\phi V_{n}$ or $\mathrm{V}_{r}$ lb (kN) |  | 60-degree ${ }^{5}$ |  | Tension $\phi N_{n}$ or $N_{r}$ |  | Shear$\phi V_{n} \text { or } V_{r}$ |  | 60-degree ${ }^{5}$ |  | Tension $\phi N_{n}$ or $N_{r}$ |  | Shear$\phi V_{n} \operatorname{or} V_{r}$ |  | 60-degree ${ }^{5}$ |  |
| 1/4 | 1-1/8 | (29) | 110 | (0.5) | 315 | (1.4) | 125 | (0.6) | 165 | (0.7) | 445 | (2.0) | 190 | (0.8) | 165 | (0.7) | 545 | (2.4) | 195 | (0.9) |
|  | 1-5/8 | (41) | 389 | (1.7) | 930 | (4.1) | 435 | (1.9) | 650 | (2.9) | 930 | (4.1) | 640 | (2.8) | 765 | (3.4) | 930 | (4.1) | 720 | (3.2) |
| 3/8 | 1-5/8 | (41) | 815 | (3.6) | 880 | (3.9) | 735 | (3.3) | 1,155 | (5.1) | 1,245 | (5.5) | 1,040 | (4.6) | 1,415 | (6.3) | 1,520 | (6.8) | 1,275 | (5.7) |
|  | 2-1/2 | (64) | 1,770 | (7.9) | 1,905 | (8.5) | 1,595 | (7.1) | 2,505 | (11.1) | 2,695 | (12.0) | 2,260 | (10.1) | 3,065 | (13.6) | 3,095 | (13.8) | 2,700 | (12.0) |
|  | 3-1/4 | (83) | 2,275 | (10.1) | 2,450 | (10.9) | 2,050 | (9.1) | 3,220 | (14.3) | 3,095 | (13.8) | 2,785 | (12.4) | 3,945 | (17.6) | 3,095 | (13.8) | 3,150 | (14.0) |
| 1/2 | 2-1/4 | (57) | 1,305 | (5.8) | 1,410 | (6.3) | 1,180 | (5.2) | 1,850 | (8.2) | 1,990 | (8.9) | 1,670 | (7.4) | 2,265 | (10.1) | 2,440 | (10.9) | 2,045 | (9.1) |
|  | 3 | (76) | 2,215 | (9.9) | 2,385 | (10.6) | 2,000 | (8.9) | 3,130 | (13.9) | 3,375 | (15.0) | 2,825 | (12.6) | 3,835 | (17.1) | 4,130 | (18.4) | 3,460 | (15.4) |
|  | 4-1/4 | (108) | 3,375 | (15.0) | 4,910 | (21.8) | 3,350 | (14.9) | 5,700 | (25.4) | 4,910 | (21.8) | 4,730 | (21.0) | 6,980 | (31.1) | 4,910 | (21.8) | 5,310 | (23.6) |
| 5/8 | 3-1/4 | (83) | 2,900 | (12.9) | 3,120 | (13.9) | 2,615 | (11.6) | 4,100 | (18.2) | 4,415 | (19.6) | 3,700 | (16.5) | 5,025 | (22.4) | 5,410 | (24.1) | 4,530 | (20.2) |
|  | 5 | (127) | 3,960 | (17.6) | 6,735 | (30.0) | 4,095 | (18.2) | 8,485 | (37.8) | 6,735 | (30.0) | 6,805 | (30.3) | 10,390 | (46.2) | 6,735 | (30.0) | 7,615 | (33.9) |
| 3/4 | 4 | (102) | 3,340 | (14.9) | 8,435 | (37.5) | 3,765 | (16.8) | 5,540 | (24.7) | 9,995 | (44.5) | 5,815 | (25.9) | 6,785 | (30.2) | 9,995 | (44.5) | 6,755 | (30.1) |
|  | 6-1/4 | (159) | 8,355 | (37.2) | 9,995 | (44.5) | 7,810 | (34.8) | 11,820 | (52.6) | 9,995 | (44.5) | 9,735 | (43.3) | 14,475 | (64.4) | 9,995 | (44.5) | 10,925 | (48.6) |

 an explanation of how values were determined.

 are based on testing.
 D.
 the Description of Technical Data section with the tabulated tension and shear design strengths (factored resistances).

## Table 3 - Reused Hilti KWIK HUS design strength (factored resistance) with the Hilti Reusability Gauge in uncracked concrete ${ }^{1,2}$ IMPORTANT: these values are reduced as compared to a single-use anchor

| Nominal anchor diameter in. | Nominal embedment in. (mm) |  | $\begin{gathered} \mathbf{f}^{\prime}=2000 \mathrm{psi} \\ (13.7 \mathrm{MPa}) \end{gathered}$ |  |  |  |  |  | $\begin{gathered} \mathbf{f}^{\prime}=4000 \mathrm{psi} \\ (27.5 \mathrm{MPa}) \end{gathered}$ |  |  |  |  |  | $\begin{gathered} \mathbf{f}^{\prime}=6000 \mathrm{psi} \\ (41.2 \mathrm{MPa}) \end{gathered}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Tension $\phi N_{n}$ or $N_{r}$ <br> lb <br> (kN) |  | Shear $\phi V_{n}$ or $V_{r}$ lb (kN) |  | 60-degree ${ }^{5}$ |  | Tension $\phi N_{n}$ or $N_{r}$ |  | Shear $\phi V_{n}$ or $V_{r}$ |  | 60-degree ${ }^{5}$ |  | Tension $\phi N_{n}$ or $N_{r}$ |  | Shear $\phi V_{n}$ or $V_{r}$ |  | 60-degree ${ }^{5}$ |  |
| 1/4 | 1-1/8 | (29) | 106 | (0.5) | 315 | (1.4) | 125 | (0.6) | 155 | (0.7) | 445 | (2.0) | 180 | (0.8) | 155 | (0.7) | 545 | (2.4) | 185 | (0.8) |
|  | 1-5/8 | (41) | 342 | (1.5) | 930 | (4.1) | 390 | (1.7) | 575 | (2.6) | 930 | (4.1) | 585 | (2.6) | 725 | (3.2) | 930 | (4.1) | 695 | (3.1) |
| 3/8 | 1-5/8 | (41) | 670 | (3.0) | 880 | (3.9) | 645 | (2.9) | 915 | (4.1) | 1,245 | (5.5) | 890 | (4.0) | 1,100 | (4.9) | 1,520 | (6.8) | 1,075 | (4.8) |
|  | 2-1/2 | (64) | 970 | (4.3) | 1,905 | (8.5) | 1,040 | (4.6) | 1,370 | (6.1) | 2,695 | (12.0) | 1,470 | (6.5) | 2,395 | (10.7) | 3,095 | (13.8) | 2,295 | (10.2) |
|  | 3-1/4 | (83) | 2,160 | (9.6) | 2,450 | (10.9) | 1,985 | (8.8) | 2,705 | (12.0) | 3,095 | (13.8) | 2,490 | (11.1) | 2,870 | (12.8) | 3,095 | (13.8) | 2,590 | (11.5) |
| 1/2 | 2-1/4 | (57) | 955 | (4.2) | 1,410 | (6.3) | 950 | (4.2) | 1,350 | (6.0) | 1,990 | (8.9) | 1,345 | (6.0) | 1,955 | (8.7) | 2,440 | (10.9) | 1,850 | (8.2) |
|  | 3 | (76) | 1,555 | (6.9) | 2,385 | (10.6) | 1,565 | (7.0) | 2,195 | (9.8) | 3,375 | (15.0) | 2,210 | (9.8) | 3,380 | (15.0) | 4,130 | (18.4) | 3,180 | (14.2) |
|  | 4-1/4 | (108) | 3,205 | (14.3) | 4,910 | (21.8) | 3,225 | (14.4) | 5,250 | (23.4) | 4,910 | (21.8) | 4,500 | (20.0) | 5,780 | (25.7) | 4,910 | (21.8) | 4,770 | (21.2) |
| 5/8 | 3-1/4 | (83) | 2,225 | (9.9) | 3,120 | (13.9) | 2,185 | (9.7) | 3,145 | (14.0) | 4,415 | (19.6) | 3,090 | (13.8) | 4,280 | (19.0) | 5,410 | (24.1) | 4,070 | (18.1) |
|  | 5 | (127) | 3,760 | (16.7) | 6,735 | (30.0) | 3,940 | (17.5) | 7,720 | (34.4) | 6,735 | (30.0) | 6,435 | (28.6) | 6,945 | (30.9) | 6,735 | (30.0) | 6,030 | (26.8) |
| 3/4 | 4 | (102) | 2,195 | (9.8) | 6,695 | (29.8) | 2,555 | (11.4) | 3,100 | (13.8) | 6,695 | (29.8) | 3,390 | (15.1) | 6,445 | (28.7) | 6,695 | (29.8) | 5,740 | (25.5) |
|  | 6-1/4 | (159) | 7,935 | (35.3) | 9,995 | (44.5) | 7,540 | (33.6) | 11,230 | (50.0) | 9,995 | (44.5) | 9,440 | (42.0) | 12,390 | (55.1) | 9,995 | (44.5) | 10,005 | (44.5) |

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The data contained in this literature was current as of the date of publication. Updates and changes may be made based on later testing. If verification is needed that the data is still current, please contact the Hilti Technical Support Specialists at 1-800-3634458. All published load values contained in this literature represent the results of testing by Hilti or test organizations. Local base materials were used. Because of variations in materials, on-site testing is necessary to determine performance at any specific site. Laser beams represented by red lines in this publication. Printed in the United States


[^0]:     Gauge. See the Description of Technical Data section for an explanation of how values were determined.
    
     are based on testing.
     D.
     the Description of Technical Data section with the tabulated tension and shear design strengths (factored resistances).

