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Simpson Strong-Tie introduces the SBR and DBR spacer bracers for cold-formed steel construction. These spacer bracers reduce the installed cost of cold-formed steel stud walls by enabling faster stud layout while minimizing the need for bridging clips.

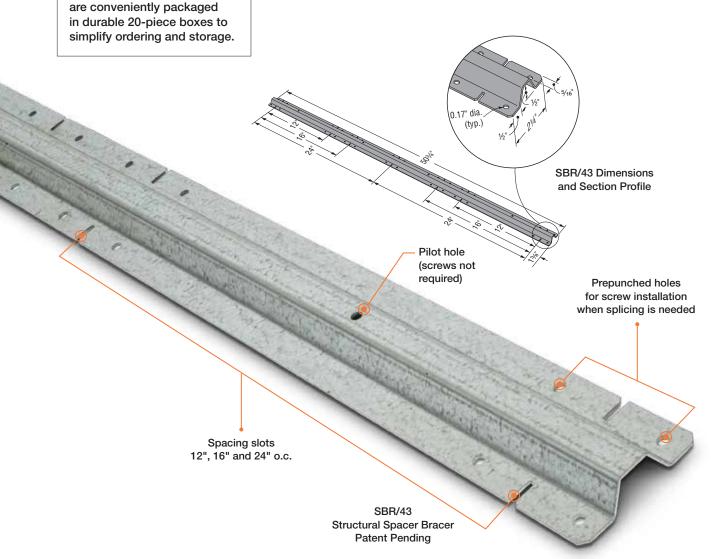
The DBR is used for interior walls to eliminate stud bow and allow for quicker drywall attachment, while the SBR is designed for structural exterior walls. Both products provide bracing along the length of the stud, and for head-of-wall slip conditions. The SBR and DBR also come with prepunched slots that eliminate the need to use bridging clips with on-module studs.

The SBR and DBR spacer bracers come with bracing load data based on assembly testing, thus mitigating risk for designers and maximizing confidence in design specs. In fact, the SBR and DBR are the only spacer bracers on the market with tabulated design values based on assembly tests.

SBR and DBR spacer bracers



SBR/43 Typical Installation





Features:

- SBR and DBR have patent-pending precisionengineered prepunched slots strategically located to enable 12", 16" and 24" on-center stud spacing and can be used to space the studs without having to mark the top track for layout.
- The SBR will accommodate 3%" and 6" studs in thicknesses of 33 mil (20 ga.) thru 68 mil (14 ga.).
- The DBR will accommodate 21/2", 35/8" and 6" studs in thicknesses of 15 mil (25 ga. EQ) through 33 mil (20 ga.).
- Prepunched holes in the SBR provide rapid screw installation when spacer-bracer splices are needed for axial load-bearing studs.
- In off-layout or end-of run conditions, the hat-section profiles enable clip attachments to the stud with Simpson Strong-Tie® LSSC or RCA connectors.

Installation:

- Spacer-bracers are fed through the stud knockout at a 90-degree angle until studs align with spacer-bracer slots. With the slots engaging the stud web, the spacerbracer is then rotated back to the flat position so that the slotted flanges are on the bottom.
- For off-layout or end-of-run studs where a spacerbracer slot does not engage a stud, manually snip the spacer-bracer flanges with a ½" deep slot and secure the spacer bracer to the stud with Simpson Strong-Tie LSSC or RCA connectors. Use all specified fasteners.



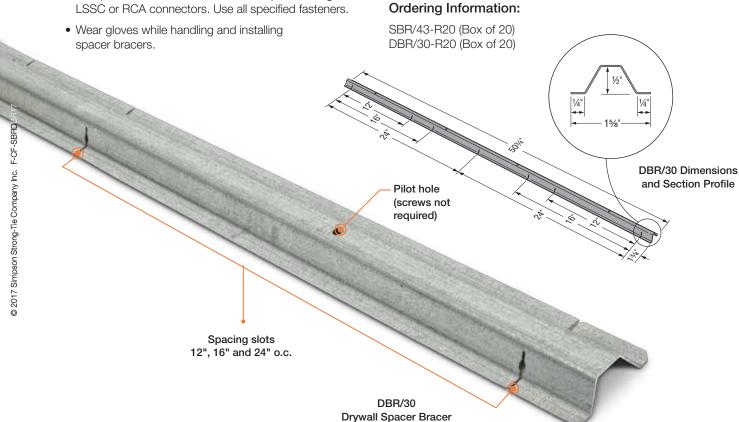
DBR/30 Typical Installation

Material: SBR/43 — 43 mil (40 ksi);

DBR/30 - 27 mil (33 ksi)

Finish: Galvanized (G90)

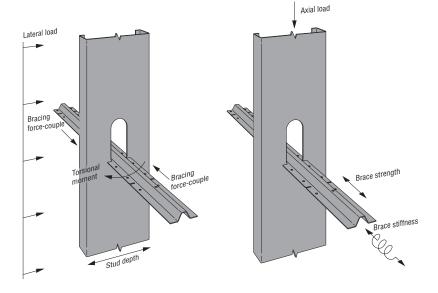
Codes: Testing performed in accordance with ICC-ES AC261. Visit stongtie.com for the latest load values and testing



Patent Pending

SBR and DBR Spacer Bracer — Connection Strength and Stiffness

Madal	Stud Stud Allowable Brace Original Brace							
Model No.	Depth (in.)	Thickness mil (ga.)	Moment (in./lb.)	Strength (lb.)	Stiffness (lb./in.)			
		33 (20)	235	390	845			
	3%	43 (18)	310	435	1,390			
		54 (16)	400	435	1,390			
SBR/43		68 (14)	400	435	1,390			
ODN/40	6	33 (20)	215	160	495			
		43 (18)	310	330	765			
		54 (16)	365	450	840			
		68 (14)	365	450	840			
		15 (25 EQ)	55	_	_			
		18 (25)	55	_	_			
	35/8	19 (20 EQ)	60	_	_			
		30 (20 DW)	85	_	_			
DBR/30		33 (20 STR)	90	_	_			
טפויטט		15 (25 EQ)	55	_	_			
		18 (25)	55	_	_			
	6	19 (20 EQ)	60	_	_			
		30 (20 DW)	85	_	_			
		33 (20 STR)	90	_	_			



Laterally Loaded C-Stud with SBR Spacer Bracer (DBR Spacer Bracer Similar)

Axially Loaded C-Stud with SBR Spacer Bracer

- Allowable loads are for use when utilizing the traditional Allowable Stress Design methodology. For LRFD loads multiply the ASD tabulated values by 1.6.
- Tabulated Allowable Brace Strengths are based on ultimate test load divided by a safety factor. Serviceability limit is not considered, as brace stiffness requirements are given in section D3.3 of AlSI S100-2012.
- 3. Tabulated Brace Stiffness values apply to both ASD and LRFD designs.
- Allowable loads consider bridging connection only. It is the responsibility of the Designer to verify the strength and serviceability of the framing members.
- 5. EQ Equivalent, DW Drywall, STR Structural.

SBR and DBR Gross Properties

Model	Design	- 4 5	Area		0 4 3	5 (1)		C (in 3) D (in)	Torsional Properties						
No.	Thickness (in.)	F _y (ksi)	(in.²)	I _x (in.⁴)	S _x (in. ³)	R _x (in.)	l _y (in.⁴)	S _y (in. ³)	R _y (in.)	Jx1,000 (in.⁴)	C _w (in. ⁶)	Y _o (in.)	m (in.)	R _o (in.)	β
SBR/43	0.0468	40	0.126	0.0047	0.1458	0.1936	0.0436	0.0400	0.5891	0.0916	5.56E-04	0.283	-0.017	0.681	0.828
DBR/30	0.0289	33	0.060	0.0023	0.0082	0.1936	0.0109	0.0141	0.4259	0.0167	7.05E-05	0.346	0.087	0.582	0.647

SBR and DBR Net Properties

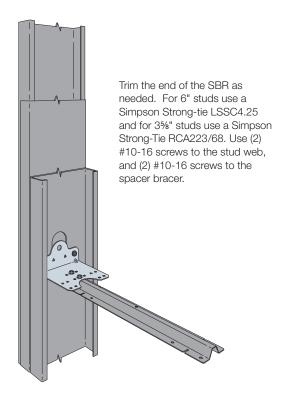
Model	Area							Torsional Properties					
No.	(in.²)	I _x (in. ⁴)	S _x (in. ³)	R _x (in.)	l _y (in.⁴)	S _y (in. ³)	R _y (in.)	Jx1,000 (in.⁴)	C _w (in.6)	Y _o (in.)	m (in.)	R _o (in.)	β
SBR/43	0.085	0.0028	0.0097	0.1816	0.0120	0.0184	0.3765	0.0617	3.43E-05	0.355	0.141	0.548	0.581
DBR/30	0.022	0.0001	0.0004	0.0479	0.0008	0.0027	0.1944	0.0061	1.09E-06	0.086	0.051	0.218	0.844

SBR and DBR Allowable Member Strengths

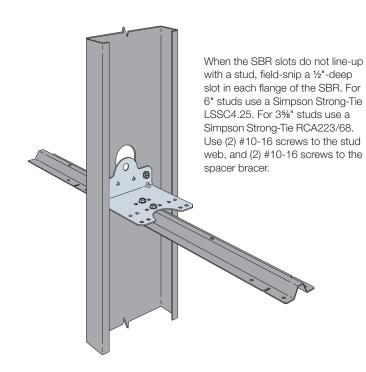
Model No.	Ma (F _y) (inlb.)	Ma (12" o.c.) (inlb.)	Ma (16" o.c.) (inlb.)	Ma (24" o.c.) (inlb.)	Pa (12" o.c.) (lb.)	Pa (16" o.c.) (lb.)	Pa (24" o.c.) (lb.)
SBR/43	369	369	369	360	945	904	618
DBR/30	44	40	38	32	_	_	_

- 1. Net section properties are based a section that excludes all material that is interrupted by the slots.
- 2. Member strengths are based on DSM Analysis (non-pregualified section, $\Omega = 2.0$).
- 3. Cb=1.67 has been applied to Ma to account for a triangular moment diagram with zero end moment.

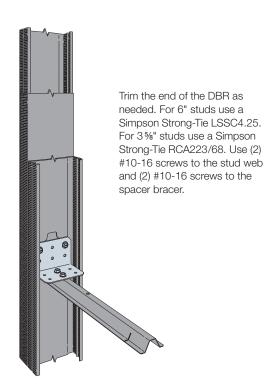




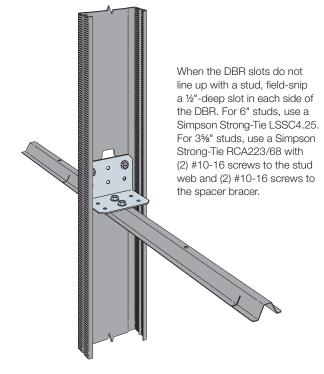
SBR End-of-Run for 6" Studs with LSSC4.25 (3%" Studs with RCA223/68 Similar)



SBR Off-Module for 6" Studs with LSSC4.25 (35%" Studs with RCA 223/68 Similar)

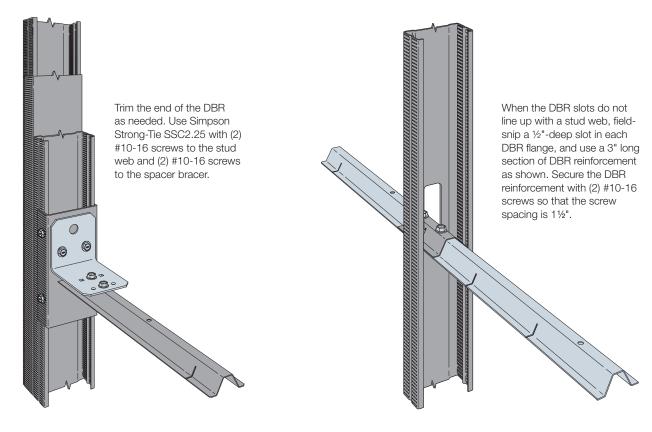


DBR End-of-Run for 3%" Studs with RCA223/68 (6" Studs with LSSC4.25 Similar)



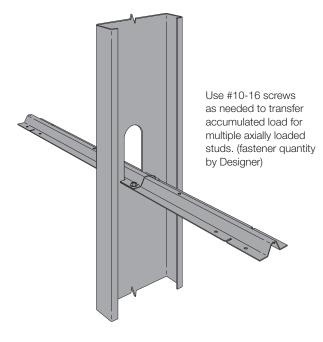
DBR Off-Module for 3%" Studs with RCA223/68 (6" Studs with LSSC4.25 Similar)





DBR End-of-Run for 2.5" Studs with SSC2.25

DBR Off-Module for 2½" Studs with DBR Reinforcement (DBR and SBR with 3%" Studs and 6" Studs Similar)



Typical SBR Splice for Axially Loaded Studs

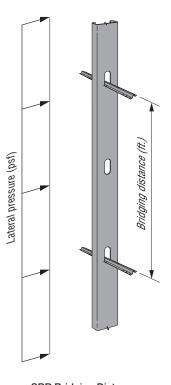
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SBR/43 Maximum Bridging Distance (ft.)

Stud	Stud	Stud Lateral Stud Pressure (psf)											
Spacing (in.)	Section	Thickness mil (ga.)	5	10	15	20	25	30	35	40	45	50	
		33 (20)	8	8	8	8	7	6	5	4	4	_	
	362S162	43 (18)	8	8	8	8	8	8	7	6	5	5	
	3023102	54 (16)	8	8	8	8	8	8	8	7	7	6	
		68 (14)	8	8	8	8	8	8	8	8	7	6	
		33 (20)	8	8	8	7	6	5	4	_	_	_	
	2626200	43 (18)	8	8	8	8	8	6	5	5	4	4	
	362S200	54 (16)	8	8	8	8	8	8	6	6	5	4	
10		68 (14)	8	8	8	8	8	8	6	6	5	4	
12		33 (20)	8	8	8	8	8	7	6	5	4	4	
	6000160	43 (18)	8	8	8	8	8	8	8	7	6	6	
	600S162	54 (16)	8	8	8	8	8	8	8	8	8	7	
	600S200	68 (14)	8	8	8	8	8	8	8	8	8	7	
		33 (20)	8	8	8	7	6	5	4	_	_	_	
		43 (18)	8	8	8	8	8	7	6	5	5	4	
		54 (16)	8	8	8	8	8	8	7	6	6	5	
		68 (14)	8	8	8	8	8	8	7	6	6	5	
		33 (20)	8	8	8	7	5	4	4	_	_	_	
	362S162	43 (18)	8	8	8	8	7	6	5	4	4		
		54 (16)	8	8	8	8	8	7	6	5	5	4	
		68 (14)	8	8	8	8	8	8	6	6	5	4	
		33 (20)	8	8	7	5	4	_	_	_	_	_	
	362S200	43 (18)	8	8	8	7	6	5	4	_	_	_	
		54 (16)	8	8	8	8	7	6	5	4	4		
4.0		68 (14)	8	8	8	8	7	6	5	4	4		
16		33 (20)	8	8	8	7	6	5	4	_			
	0000100	43 (18)	8	8	8	8	8	7	6	5	5	4	
	600S162	54 (16)	8	8	8	8	8	8	7	6	6	5	
		68 (14)	8	8	8	8	8	8	7	6	6	5	
		33 (20)	8	8	7	5	4	_	_	_	_	_	
	0000000	43 (18)	8	8	8	8	6	5	4	4	_	_	
	600S200	54 (16)	8	8	8	8	8	6	5	5	4	4	
		68 (14)	8	8	8	8	8	6	5	5	4	4	
		33 (20)	8	8	6	4							
	2626162	43 (18)	8	8	8	6	5	4					
	362S162	54 (16)	8	8	8	7	6	5	4				
		68 (14)	8	8	8	7	6	5	4	_	_	_	
		33 (20)	8	7	5	_	_	_	_	_	_	_	
	362S200	43 (18)	8	8	6	5	4		_				
	3023200	54 (16)	8	8	7	5	4	E			Ē		
24		68 (14)	8	8	7	5	4					Ε	
24		33 (20)	8	8	7	5	4						
	600S162	43 (18)	8	8	8	7	6	5	4				
	0000102	54 (16)	8	8	8	8	7	6	5	4	4		
		68 (14)	8	8	8	8	7	6	5	4	4		
		33 (20)	8	7	5	_	_	_	_	_	_		
	6000000	43 (18)	8	8	7	5	4	_	_	_	_		
	600S200	54 (16)	8	8	8	6	5	4	_	_	_	_	
		68 (14)	8	8	8	6	5	4	_	_	_		
				_							_	_	

DBR/30 Maximum Bridging Distance (ft.)

15 (25 EQ) 8 18 (25) 8 18 (25) 8 362S125 19 (20 EQ) 8 30 (20 DW) 8	Lateral Stud Pressure (psf)			
18 (25) 8 362S125 19 (20 EQ) 8 30 (20 DW) 8	10			
362S125 19 (20 EQ) 8 30 (20 DW) 8	5			
30 (20 DW) 8	5			
	5			
00 (00 OTD) 3	5			
33 (20 STR) 8	5			
15 (25 EQ) 8	6			
18 (25) 8	6			
600S125 19 (20 EQ) 8	6			
30 (20 DW) 8	6			
33 (20 STR) 8	6			
15 (25 EQ) 7	_			
18 (25) 7	_			
362S125 19 (20 EQ) 7	_			
30 (20 DW) 7	_			
33 (20 STR) 7	_			
16 15 (25 EQ) 8	4			
18 (25) 8	4			
600S125 19 (20 EQ) 8	4			
30 (20 DW) 8	4			
33 (20 STR) 8	4			
15 (25 EQ) 4	_			
18 (25) 4	_			
362S125 19 (20 EQ) 4	_			
30 (20 DW) 4	_			
33 (20 STR) 4	_			
24 15 (25 EQ) 4	_			
18 (25) 4	_			
600S125 19 (20 EQ) 4	_			
30 (20 DW) 5	_			
33 (20 STR) 5	_			



SBR Bridging Distance (DBR Similar)

- 1. Tabulated solutions are for ASD lateral pressure. Contact Simpson Strong-Tie for LRFD solutions.
- 2. Lateral pressures shall be determined based on the load combinations of the applicable building code. For designs in accordance with the 2009 IBC and earlier, wind pressures are at the working stress level and may be used directly. For designs in accordance with the 2012 and 2015 IBC, wind pressures are at the strength level and must be multiplied by 0.6 for ASD load combinations.
- Tabulated values are based on the minimum of the tested connection strength and the calculated SBR/DBR member strength. Studs must be checked separately for unbraced length.



Given

- 2015 IBC (ASCE 7-10 and AISI S100-2012)
- 600S162-54 (50 ksi) studs at 24" o.c., 10' stud height
 - o Mid-point bracing (5' o.c.)
 - o Distance from shear center to mid-plane of web, m = 0.663 in. (2013 AISI Manual, Table I-2)
- Wind design pressure = 34 psf
- P_{ra} = Required ASD axial load = 3,000 lb.

Axially Loaded Stud

Required brace strength (AISI S100, Eq. D3.3-1)

$$P_{rb} = 0.01P_{ra} = (0.01)(3,000 \text{ lb.}) = 30 \text{ lb.}$$

Required brace stiffness (AISI S100, Eq. D3.3-2a)

$$\beta_{rb} = (2[4-(2/n)]/L_b)(\Omega P_{ra}) = (2[4-(2/n)]/60)(2)(3,000) = 400 \text{ lb./in.}$$

Check connection strength and stiffness from Strength and Stiffness table (page 4) for the SBR/43 for 6" deep, 54 mil studs

- ➤ Allowable brace strength = 450 lb. > 30 lb. OK
- Allowable brace stiffness = 840 lb./in. > 400 lb./in. OK

Check member strength from Allowable Strengths table (page 4) for the SBR/43 for 24" o.c.

Note: Member stiffness and the effects of accumulated load for multiple axially loaded studs have not been accounted for in the above calculations. Reference CFSEI Tech Note W400-16 for additional guidance on these topics.

Laterally Loaded Stud

ASD Design load tributary to brace:

W = (0.6)(34 psf)(2 ft.)(5 ft.) = 204 lb.

Note: 2015 IBC load combinations for

ASD include a factor of 0.6

Required flange force (AISI S100 Eq. D3.2.1-3)

$$P_{1.1} = -P_{1.2} = 1.5 \text{ (m/d)} W = (1.5)(0.663 \text{ in./6 in.)} (204 \text{ lb.}) = 33.8 \text{ lb.}$$

Torsional moment

$$M_z = P_{L1}d = -P_{L2}d = (33.8)(6) = 202.8 \text{ in.-lb.}$$

Moment applied to bridging member

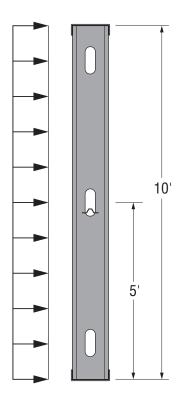
$$M_{\rm m} = 0.64 M_{\rm z} = (0.64)(202.8) = 129.8 \ {\rm in.-lb.}$$

Note: The 0.64 factor is from an analysis of a five-span continuous beam that is loaded with equal support moments (Reference AISI Design Guide D110-07, page 2-9, Figure 2-6)

Check connection strength from Strength and Stiffness table (page 4) for the SBR/43 for 6° deep, 54 mil studs

Allowable torsional moment = 365 in.-lb. > 202.8 in.-lb. OK

Check member strength from Allowable Strengths table (page 4) for the SBR/43 for 24 " o.c.



Combined-Loading Check of Connection

 $(P_{br}/Allowable~brace~strength) + (M_z/Allowable~torsional~moment) \leq 1.0 (30 lb./450 lb.) + (202.8 in.-lb./365 in.-lb.) = 0.62 < 1.0 <math display="inline">\bf OK$

Combined-Loading Check of Bridging Member

Reference AISI Eqs. C5.2.1-1, C5.2.1-2, or Eq. C52.1-3 as applicable. For this condition, Eq. C5.2.1-3 applies.

$$\frac{\Omega_c P}{P_a} + \frac{\Omega_b M}{M_a} \le 1.0$$

$$P_n = 2P_a$$
 $M_n = 2M_a$

$$\frac{1.8 (30)}{2 (618)} + \frac{1.67 (129.8)}{2 (360)} = 0.34 < 1.0$$
 OK

Note: The allowable strengths given in the Allowable Strengths table (page 4) have been converted to nominal strengths by multiplying by Ω =2.0.