The Titen HD stainless-steel screw anchor for concrete and masonry is ideal for when the job calls for fast and efficient installation in multiple types of environments. The Titen HD stainless steel is a state-of-the-art anchor solution that combines the long-lasting corrosion resistance of Type 300 Series stainless steel with the undercutting ability of heat-treated carbon-steel cutting threads.
Innovative - The serrated carbon-steel threads on the tip of the stainless-steel Titen HD are vital because they undercut the concrete as the anchor is driven into the hole, making way for the rest of the threads to interlock with the concrete. In order for these threads to be durable enough to cut into the concrete, they are formed from carbon steel that is then hardened and brazed onto the tip of the anchor.
Corrosion Resistant - For dry, interior applications, carbon-steel corrosion is not a risk, but in any kind of exterior, coastal or chemical environment stainless steel provides the best solution for corrosion protection.

## Features:

- Ideal for exterior or corrosive environments
- Installs with an impact wrench or with a hand tool
- Tested per ACI355.2, AC193 and AC106

Codes: IAPMO UES ER-493 (concrete);
ICC-ES ESR-1056 (masonry);
City of LA Supplement within ER-493 (concrete); City of LA Supplement within ESR-1056 (masonry); Florida FL15730 (masonry); FL16230 (concrete)
Material: Type 316 and Type 304 stainless steel.
See pp. 235-236 or visit strongtie.com/info for more corrosion information.

## Installation

(1) Caution: Holes in steel fixtures to be mounted should match the diameter specified in the table below if steel is thicker than 12 gauge.
( Caution: Use a Titen HD screw anchor one time only - installing the anchor multiple times may result in excessive thread wear and reduce load capacity Do not use impact wrenches to install into hollow CMU.
! Caution: Oversized holes in base material will reduce or eliminate the mechanical interlock of the threads with the base material and reduce the anchor's load capacity.

1. Drill a hole in the base material using a carbide drill bit (complying with ANSI B212.15) with the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to the specified minimum hole depth overdrill (see table below) to allow the thread tapping dust to settle, and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate embedment depth and the dust from drilling and tapping.
2. Insert the anchor through the fixture and into the hole.
3. Tighten the anchor into the base material until the hex-washer head or the countersunk head contacts the fixture.

Additional Installation Information

| Titen HD <br> Diameter <br> (in.) | Wrench <br> Size <br> (in.) | Recommended <br> Steel Fixture <br> Hole Size <br> (in.) | Minimum <br> Hole Depth <br> Overdrill <br> (in.) |
| :---: | :---: | :---: | :---: |
| $1 / 4$ | $3 / 8$ | $3 / 8$ to $7 / 16$ | $1 / 8$ |
| $3 / 8$ | $9 / 16$ | $1 / 2$ to $9 / 16$ | $1 / 4$ |
| $1 / 2$ | $3 / 4$ | $5 / 8$ to $11 / 16$ | $1 / 2$ |
| $5 / 8$ | $15 / 16$ | $3 / 4$ to $13 / 16$ | $1 / 2$ |
| $3 / 4$ | $11 / 8$ | $7 / 8$ to $15 / 16$ | $1 / 2$ |

[^0]

Innovative Carbon-Steel Lead Threads

Installation Sequence



Stainless-Steel Titen HD Hex-Washer Head Style Screw Anchor

US Patents 8,747,042 B2 and $9,517,519$

Minimum overdrill. See table.

## Stainless-Steel Countersunk Head Style

The countersunk head style is for applications that require a flush-mount profile. Countersinking also leaves a cleaner surface appearance for exposed through-set applications. The anchor head's 6-lobe drive eases installation and is less prone to stripping than traditional recessed anchor heads.

## Features

- Available in many standard lengths in $1 / 4$ " and $3 / 8^{"}$ diameters
- Countersunk head allows screw anchor applications incompatible with a hex head
- Countersunk version includes (1) driver bit in each box

Codes: IAPMO UES ER-493 (concrete);
ICC-ES ESR-1056 (masonry);
City of LA Supplement within ER-493 (concrete);
City of LA Supplement within ESR-1056 (masonry);
Florida FL15730 (masonry); FL16230 (concrete)
Material: Type 316 stainless steel with carbon-steel lead threads

Additional Installation Information

| Titen HD <br> Diameter <br> (in.) | Bit <br> Size | Recommended <br> Steel Fixture <br> Hole Size <br> (in.) | Minimum <br> Hole Depth <br> Overdrill <br> (in.) |
| :---: | :---: | :---: | :---: |
| $1 / 4$ | T30 | $3 / 8$ to $7 / 16$ | $1 / 8$ |
| $3 / 8$ | T50 | $1 / 2$ to 916 | $1 / 4$ |

Suggested fixture hole sizes are for structural steel thicker than 12 gauge only. Larger holes are not required for wood or thinner cold-formed steel members.


Stainless-Steel Titen HD Countersunk Head Style Screw Anchor

Installation Sequence



Titen HD Countersunk Installation

Stainless-Steel Titen HD Anchor Product Data - Hex Washer Head

| Size <br> (in.) | Model No. <br> (Type 316) | Model No. <br> (Type 304) | Thread <br> Length <br> (in.) | Drill Bit <br> Diameter <br> (in.) | Wrench <br> Size <br> (in.) | Quantity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

$\dagger$ Does not meet minimum embedment in code report.

1. Anchor length is measured from under head to bottom of anchor.

Stainless-Steel Titen HD Anchor Product Data - Countersunk

| Size <br> (in.) | Model No. <br> (Type 316) | Thread <br> Length <br> (in.) | Drill Bit <br> Diameter <br> (in.) | Bit <br> Size | Quantity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

[^1]
## Stainless-Steel Titen HD ${ }^{\circledR}$ Design Information - Concrete

Stainless-Steel Titen HD Installation Information ${ }^{1}$
IBC


| Characteristic | Symbol | Units | Nominal Anchor Diameter (in.) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $1 / 4$ |  | $3 / 8$ |  | $1 / 2$ |  |  | 5/8 |  | $3 / 4$ |  |
| Installation Information |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Nominal Diameter | $d_{a}$ | in. | $1 / 4$ |  | $3 / 8$ |  | 1/2 |  |  | 5/8 |  | $3 / 4$ |  |
| Drill Bit Diameter | $d_{\text {bit }}$ | in. | $1 / 4$ |  | $3 / 8$ |  | $1 / 2$ |  |  | 5/8 |  | $3 / 4$ |  |
| Minimum Baseplate Clearance Hole Diameter ${ }^{2}$ | $d_{c}$ | in. | $3 / 8$ |  | 1/2 |  | 5/8 |  |  | $3 / 4$ |  | 7/8 |  |
| Maximum Installation Torque ${ }^{3}$ | $T_{\text {inst,max }}$ | ft. - lbf | N/A |  | 40 |  | 70 |  |  | 85 |  | 150 |  |
| Maximum Impact Wrench Torque Rating | $T_{\text {impact,max }}$ | ft.-lbf | 125 |  | 150 |  | 345 |  |  | 345 |  | 380 |  |
| Minimum Hole Depth | $h_{\text {hole }}$ | in. | $21 / 4$ | $31 / 8$ | $23 / 4$ | 3112 | $33 / 4$ |  | 4112 | 4112 | 6 | 6 | $63 / 4$ |
| Nominal Embedment Depth | $h_{\text {nom }}$ | in. | 21/8 | 3 | $2^{1 / 2}$ | 3114 | $31 / 4$ |  | 4 | 4 | $51 / 2$ | $51 / 2$ | $61 / 4$ |
| Effective Embedment Depth | $h_{e t}$ | in. | 1.27 | 2.01 | 1.40 | 2.04 | 1.86 |  | 2.50 | 2.31 | 3.59 | 3.49 | 4.13 |
| Critical Edge Distance | $C_{a c}$ | in. | 3 | 3 | $41 / 2$ | $51 / 2$ | 6 |  | $53 / 4$ | 6 | 63/8 | $63 / 4$ | 73/8 |
| Minimum Edge Distance | $C_{\text {min }}$ | in. | $11 / 2$ | $11 / 2$ | $13 / 4$ | $13 / 4$ | $13 / 4$ | $21 / 4$ | $13 / 4$ | $13 / 4$ | $13 / 4$ | $13 / 4$ | $13 / 4$ |
| Minimum Spacing | $S_{\text {min }}$ | in. | $11 / 2$ | $11 / 2$ | 3 | 3 | 4 | 3 | 3 | 3 | 3 | 3 | 3 |
| Minimum Concrete Thickness | $h_{\text {min }}$ | in. | $31 / 2$ | $43 / 8$ | 4 | 5 |  |  | $61 / 4$ | 6 | $81 / 2$ | 83/4 | 10 |
| Anchor Data |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Yield Strength | $f_{y a}$ | psi | 88,000 |  | 98,400 |  | 91,200 |  |  | 83,200 |  | 92,000 |  |
| Tensile Strength | $f_{u t a}$ | psi | 110,000 |  | 123,000 |  | 114,000 |  |  | 104,000 |  | 115,000 |  |
| Minimum Tensile and Shear Stress Area | $A_{s e}$ | in. ${ }^{2}$ | 0.0430 |  | 0.099 |  | 0.1832 |  |  | 0.276 |  | 0.414 |  |
| Axial Stiffness in Service Load Range - Uncracked Concrete | $\beta_{\text {uncr }}$ | lb./in. | 139,300 |  | 807,700 |  | 269,085 |  |  | 111,040 |  | 102,035 |  |
| Axial Stiffness in Service Load Range - Cracked Concrete | $\beta_{\text {cr }}$ | $\mathrm{lb} . / \mathrm{in}$. | 103,500 |  | 113,540 |  | 93,675 |  |  | 94,400 |  | 70,910 |  |

For SI: $1 \mathrm{in} .=25.4 \mathrm{~mm}, 1 \mathrm{ft} .-\mathrm{lbf}=1.356 \mathrm{~N}-\mathrm{m}, 1 \mathrm{psi}=6.89 \mathrm{kPa}, 1 \mathrm{in} .^{2}=645 \mathrm{~mm}^{2}, 1 \mathrm{lb} . / \mathrm{in} .=0.175 \mathrm{~N} / \mathrm{mm}$.

1. The information presented in this table is to be used in conjunction with the design criteria of ACl 318 -19 Chapter 17, ACl 318-14 Chapter 17 or ACl 318-11 Appendix D, as applicable.
2. The minimum hole size must comply with applicable code requirements for the connected element.
3. $T_{\text {inst,max }}$ applies to installations using a calibrated torque wrench.

Stainless－Steel Titen HD Tension Strength Design Data ${ }^{1,5}$

| Characteristic | Symbol | Units | Nominal Anchor Diameter（in．） |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $1 / 4$ |  | 3／8 |  | 1／2 |  | 5／8 |  | $3 / 4$ |  |
| Anchor Category | 1,2 or 3 | － | 3 |  | 1 |  |  |  |  |  |  |  |
| Nominal Embedment Depth | $h_{\text {nom }}$ | in． | 21／8 | 3 | $21 / 2$ | $31 / 4$ | $31 / 4$ | 4 | 4 | $51 / 2$ | $51 / 2$ | 6114 |
| Steel Strength in Tension（ACI 318－19 17．6．1，ACI 318－14 17．4．1 or ACI 318－11 Section D．5．1） |  |  |  |  |  |  |  |  |  |  |  |  |
| Tension Resistance of Steel | $N_{s a}$ | lbf | 4，730 |  | 12，177 |  | 20，885 |  | 28，723 |  | 47，606 |  |
| Strength Reduction Factor－Steel Failure ${ }^{2}$ | $\phi_{s a}$ | － | 0.75 |  |  |  |  |  |  |  |  |  |
| Concrete Breakout Strength in Tension（ACI 318－19 17．6．2，ACI 318－14 17．4．2 or ACI 318 Section D．5．2） |  |  |  |  |  |  |  |  |  |  |  |  |
| Effective Embedment Depth | $h_{\text {ef }}$ | in． | 1.27 | 2.01 | 1.40 | 2.04 | 1.86 | 2.50 | 2.31 | 3.59 | 3.49 | 4.13 |
| Critical Edge Distance | $C_{a c}$ | in． | 3 | 3 | 4112 | $51 / 2$ | 6 | $53 / 4$ | 6 | 63／8 | 63／4 | $73 / 8$ |
| Effectiveness Factor－Uncracked Concrete | $k_{\text {uncr }}$ | － | 24 | 24 | 27 | 24 | 27 | 24 | 24 | 24 | 27 | 27 |
| Effectiveness Factor－Cracked Concrete | $k_{c r}$ | － | 17 | 17 | 21 | 17 | 17 | 17 | 17 | 17 | 17 | 21 |
| Modification Factor | $\Psi_{C, N}$ | － | 1 |  |  |  |  |  |  |  |  |  |
| Strength Reduction Factor－Concrete Breakout Failure ${ }^{3}$ | $\phi_{c b}$ | － | 0.45 |  | 0.65 |  |  |  |  |  |  |  |
| Pullout Strength in Tension（ACI 318－19 17．6．3，ACl 318－14 17．4．3 or ACI 318－11 Section D．5．3） |  |  |  |  |  |  |  |  |  |  |  |  |
| Pullout Resistance Uncracked Concrete（ $\left.\mathrm{f}^{\prime}{ }_{\mathrm{c}}=2,500 \mathrm{psi}\right)$ | $N_{p, \text { uncr }}$ | lbf | 1，725 ${ }^{5}$ | 3，550 ${ }^{8}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | 3，820 ${ }^{5}$ | 9，080 ${ }^{7}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ |
| Pullout Resistance Cracked Concrete（ $\mathrm{f}_{\mathrm{c}}{ }_{\mathrm{c}}=2,500 \mathrm{psi}$ ） | $N_{p, c r}$ | lbf | $695{ }^{5}$ | 1，225 ${ }^{\text {a }}$ | 1，675 ${ }^{5}$ | $2,415^{5}$ | 1，995 ${ }^{5}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ |
| Strength Reduction Factor－Pullout Failure ${ }^{6}$ | $\phi_{p}$ | － | 0.45 |  | 0.65 |  |  |  |  |  |  |  |
| Tension Strength for Seismic Applications（ACI 318－19 17．10．3，ACI 318－14 17．2．3．3 or ACI 318－11 Section D．3．3．3） |  |  |  |  |  |  |  |  |  |  |  |  |
| Nominal Pullout Strength for Seismic Loads（ $\mathrm{f}^{\prime}{ }_{\mathrm{C}}=2,500 \mathrm{psi}$ ） | $N_{p, e q}$ | lbf | $695{ }^{5}$ | 1，225 ${ }^{5}$ | 1，675 ${ }^{5}$ | $2,415^{5}$ | 1，995 ${ }^{5}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ | N／A ${ }^{4}$ |
| Strength Reduction Factor for Pullout Failure ${ }^{6}$ | $\phi_{e q}$ | － |  | ． 45 |  |  |  |  | 65 |  |  |  |

For SI： $1 \mathrm{in} .=25.4 \mathrm{~mm}, 1 \mathrm{ft} .-\mathrm{lbf}=1.356 \mathrm{~N}-\mathrm{m}, 1 \mathrm{psi}=6.89 \mathrm{kPa}, 1 \mathrm{in}^{2}=645 \mathrm{~mm}^{2}, 1 \mathrm{lb} . / \mathrm{in} .=0.175 \mathrm{~N} / \mathrm{mm}$ ．
1．The information presented in this table is to be used in conjunction with the design criteria of ACl 318 －19 Chapter 17， ACI 318－14 Chapter 17 or ACl 318－11 Appendix D，as applicable．
2．The tabulated value of $\phi_{s a}$ applies when the load combinations of Section 1605.1 of the 2021 IBC，Section 1605.2 of the 2018，2015，2012，and 2009 IBC， ACl 318 －19 and ACl 318 －14 Section 5．3，or $\mathrm{ACI} 318-11$ Section 9.2 are used，as applicable． If the load combinations of $\mathrm{ACl} 318-11$ Appendix C are used，the appropriate value of $\phi$ must be determined in accordance with ACl 318 D．4．4（b），as applicable．
3．The tabulated values of $\phi_{c b}$ applies when both the load combinations of Section 1605.1 of the 2021 IBC，Section 1605.2 of the 2018，2015，2012，and 2009 IBC， $\mathrm{ACl} 318-19$ and $\mathrm{ACI} 318-14$ Section 5．3，or $\mathrm{ACI} 318-11$ Section 9.2 are used，as applicable， are used and the requirements of $\mathrm{ACl} 318-19$ Section 17．5．3 and Table 17．5．3（b），ACI 318－14 17．3．3（c）or ACI 318－11 D．4．3（c） for Condition B are met．Condition B applies where supplementary reinforcement is not provided in concrete．For installations where complying reinforcement can be verified，the $\phi_{c b}$ factors described in ACl 318 －19 Table 17．5．3（b）， ACl 318－14 17．3．3（c）or ACl 318－11 D．4．3（c），as applicable，may be used for Condition A．If the load combinations of $\mathrm{ACl} 318-11$ Appendix C are used， the appropriate value of $\phi$ must be determined in accordance with ACI 318－11 D．4．4（c）for Condition B．
4．N／A denotes that pullout resistance does not govern and does not need to be considered．
5．The characteristic pullout resistance for greater compressive strengths may be increased by multiplying the tabular value by（ $\left.f_{\mathrm{c}}^{\mathrm{c}} / 2,500\right)^{0.5}$ ．
6．The tabulated values of $\phi_{p}$ or $\phi_{e q}$ applies when both the load combinations of ACI 318－19 Section 5．3，ACI 318－14 Section 5.3 or ACI 318－11 Section 9．2，as applicable，are used and the requirements of ACI 318－19 Section 17．5．3 and Table 17．5．3（b）， ACl 318－14 17．3．3（c）or $\mathrm{ACl} 318-11$ D．4．3（c）for Condition B are met．If the load combinations of ACl 318 －11 Appendix C are used， the appropriate value of $\phi$ must be determined in accordance with ACl 318 －11 D．4．4（c）for Condition B．
7．The characteristic pullout resistance for greater compressive strengths may be increased by multiplying the tabular value by $\left(f_{c}^{\prime} / 2,500\right)^{0.4}$ ．
8．The characteristic pullout resistance for greater compressive strengths may be increased by multiplying the tabular value by $\left(\mathrm{f}_{\mathrm{c}} \mathrm{c} / 2,500\right)^{0.3}$ ．

## Stainless-Steel Titen HD ${ }^{\oplus}$ Design Information - Concrete

Stainless-Steel Titen HD Shear Strength Design Data ${ }^{1}$
IBC


| Characteristic | Symbol | Units | Nominal Anchor Diameter (in.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/4 |  | 3/8 |  | 1/2 |  | 5/8 |  | $3 / 4$ |  |
| Anchor Category | 1,2 or 3 | - | 3 |  | 1 |  |  |  |  |  |  |  |
| Nominal Embedment Depth | $h_{\text {nom }}$ | in. | 21/8 | 3 | $21 / 2$ | $31 / 4$ | $31 / 4$ | 4 | 4 | $51 / 2$ | $51 / 2$ | 6114 |

Steel Strength in Shear (ACI 318-19 17.7.1, ACI 318-14 17.5.1 or ACI 318-11 Section D.6.1)

| Shear Resistance of Steel | $V_{s a}$ | lbf | 2,285 | 3,790 | 4,780 | 6,024 | 7,633 | 10,422 | 10,649 | 13,710 | 19,161 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Strength Reduction Factor - Steel Failure ${ }^{2}$ | $\phi_{s a}$ | - | 0.65 |  |  |  |  |  |  |  |  |

Concrete Breakout Strength in Shear (ACI 318-19 17.7.2, ACI 318-14 17.5.2 or ACI 318-11 Section D.6.2)

| Nominal Diameter | $d_{a}$ | in. | 0.250 |  | 0.375 |  | 0.500 |  | 0.625 |  | 0.750 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load Bearing Length of Anchor in Shear | Ie | in. | 1.27 | 2.01 | 1.40 | 2.04 | 1.86 | 2.50 | 2.31 | 3.59 | 3.49 | 4.13 |
| Strength Reduction Factor - Concrete Breakout Failure ${ }^{3}$ | $\phi_{c b}$ | - | 0.70 |  |  |  |  |  |  |  |  |  |

Concrete Pryout Strength in Shear (ACI 318-19 17.7.3, ACI 318-14 17.5.3 or ACI 318-11 Section D.6.3)

| Coefficient for Pryout Strength | $k_{c p}$ | - | 1.0 |  |  |  |  | 2.0 | 1.0 | 2.0 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Strength Reduction Factor - Concrete Pryout Failure ${ }^{3}$ | $\phi_{C p}$ | - | 0.70 |  |  |  |  |  |  |  |  |  |
| Shear Strength for Seismic Applications (ACI 318-19 17.10.3, ACI 318-14 17.2.3.3 or ACl 318-11 Section D.3.3.3) |  |  |  |  |  |  |  |  |  |  |  |  |
| Shear Resistance - Single Anchor for Seismic Loads ( $\mathrm{f}^{\prime} \mathrm{c}=2,500 \mathrm{psi}$ ) | $V_{s a, e q}$ | lbf | 1,370 | 1,600 | 3,790 | 4,780 | 5,345 | 6,773 | 9,367 | 9,367 | 10,969 | 10,969 |
| Strength Reduction Factor - Steel Failure ${ }^{2}$ | $\phi_{e q}$ | - | 0.65 |  |  |  |  |  |  |  |  |  |

For SI: $1 \mathrm{in} .=25.4 \mathrm{~mm}, 1 \mathrm{lbf}=4.45 \mathrm{~N}$.

1. The information presented in this table is to be used in conjunction with the design criteria of ACl 318 -19 Chapter 17, ACl 318-14 Chapter 17 or ACl 318-11 Appendix D, as applicable.
2. The tabulated value of $\phi_{s a}$ and $\phi_{e q}$ applies when the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015, 2012, and 2009 IBC, ACl 318-19 or ACl 318 -14 Section 5.3, or $\mathrm{ACl} 318-11$ Section 9.2, as applicable, are used. If the load combinations of ACl 318-11 Appendix C are used, the appropriate value of $\phi_{s a}$ and $\phi_{e q}$ must be determined in accordance with ACl 318-11 D.4.4(b).
3. The tabulated values of $\phi_{c b}$ and $\phi_{C D}$ apply when both the load combinations of Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015, 2012, and 2009 IBC, $\operatorname{ACl} 318-19$ or $\mathrm{ACl} 318-14$ Section 5.3 or $\mathrm{ACl} 318-11$ Section 9.2 are used and the requirements of ACl 318-19 Section 17.5.3 and Table 17.5.3(b), ACl 318-14 Section 1703.3, or ACI 318-11 D.4.3(c) for Supplementary reinforcement are not present (Condition B) are met. Condition B applies where supplementary reinforcement is not provided in concrete. For installations where complying reinforcement is verified, the $\phi_{c b}$ and $\phi_{c p}$ factors described in ACl 318-19 Table 17.5.3(b), ACI 318-14 17.3.3(c), or ACI 318-11 D.4.3(c), as applicable, may be used for Condition A. If the load combinations of $\mathrm{ACl} 318-11$ Appendix C are used, the appropriate value of $\phi_{c b}$ shall be determined in accordance with $\mathrm{ACl} 318-11$ D.4.5(c) for Condition B.

## Stainless-Steel Titen HD ${ }^{\circledR}$ Design Information - Concrete

Stainless-Steel Titen HD Screw Anchor Setting Information for Installation IBC A $\vec{A}$ on the Top of Concrete-Filled Profile Steel Deck Floor and Roof Assemblies ${ }^{1,2,3,4}$

| Design Information | Symbol | Units | Nominal Anchor Diameter (in.) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $1 / 4$ | $3 / 8$ | 1/2 |
| Nominal Embedment Depth | $h_{\text {nom }}$ | in. | $21 / 8$ | $21 / 2$ | $31 / 4$ |
| Effective Embedment Depth | $h_{\text {ef }}$ | in. | 1.27 | 1.40 | 1.86 |
| Minimum Concrete Thickness ${ }^{5}$ | $h_{\text {min,deck }}$ | in. | $21 / 2$ | 3114 | $33 / 4$ |
| Critical Edge Distance | $C_{\text {ac, deck, top }}$ | in. | 3 | $41 / 2$ | $71 / 2$ |
| Minimum Edge Distance | $C_{\text {min,deck,top }}$ | in. | $11 / 2$ | $13 / 4$ | $13 / 4$ |
| Minimum Spacing | $S_{\text {min,deck,top }}$ | in. | $11 / 2$ | 3 | 3 |

For SI: $1 \mathrm{in} .=25.4 \mathrm{~mm}, 1 \mathrm{lbf}=4.45 \mathrm{~N}$.

1. For anchors installed in the topside of concrete-filled deck assemblies, as shown in Figure 1, the nominal concrete breakout strength of a single anchor or group of anchors in shear, $V_{c b}$ or $V_{c b g}$, respectively, must be calculated in accordance with $\mathrm{ACl} 318-19$ Section 17.7.2, $\mathrm{ACI} 318-14$ Section 17.5.2 or $\mathrm{ACI} 318-11$ Section D.6.2, using the actual member thickness, $h_{\text {min, deck, }}$, in the determination of $A_{v c}$.
2. Design capacity shall be based on calculations according to values in the tables featured on pp. 84-85.
3. Minimum flute depth (distance from top of flute to bottom of flute) is $1 \frac{1}{2 \prime \prime}$ (see Figure 1 ).
4. Steel deck thickness shall be minimum 20 gauge.
5. Minimum concrete thickness ( $h_{\text {min, deck }}$ ) refers to concrete thickness above upper flute (see Figure 1).


Figure 1. Installation of $1 / 4 "-, 3 / 8^{\prime \prime}-$ and $1 / 2 "-D i a m e t e r$ Anchors in the Topside of Concrete over Steel Deck

Stainless-Steel Titen HD Allowable Tension and Shear Loads in 8" Medium-Weight and Normal-Weight Grout-Filled CMU

| $\begin{gathered} \text { Size } \\ \text { in. } \\ (\mathrm{mm}) \end{gathered}$ | Drill Bit Diameter in. | Minimum Embedment Depth in. (mm) | Critical Edge Distance $\mathrm{C}_{\text {crit }}$ in. (mm) | Minimum Edge Distance $\mathrm{C}_{\text {min }}$ in. (mm) | Critical Spacing Distance in. (mm) | Values for $8^{\prime \prime}$ Medium-Weight or Normal-Weight Grout-Filled CMU |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Tension Load |  | Shear Load |  |
|  |  |  |  |  |  | Ultimate <br> lb. (kN) | Allowable <br> lb. (kN) | Ultimate <br> lb. (kN) | Allowable <br> lb. (kN) |
| Anchor Installed in the Face of the CMU Wall (See Figure 1) |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} 1 / 4 \\ (6.4) \end{gathered}$ | $1 / 4$ | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 11 / 4 \\ & (32) \end{aligned}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 1,325 \\ (5.9) \end{gathered}$ | $\begin{array}{r} 265 \\ (1.2) \end{array}$ | $\begin{gathered} 1,400 \\ (6.2) \end{gathered}$ | $\begin{aligned} & 280 \\ & (1.3) \end{aligned}$ |
| $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | 3/8 | 23/4 <br> (70) | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{gathered} 2,125 \\ (9.5) \end{gathered}$ | $\begin{aligned} & 425 \\ & (1.9) \end{aligned}$ | $\begin{aligned} & 2,850 \\ & (12.7) \end{aligned}$ | $\begin{array}{r} 570 \\ (2.5) \end{array}$ |
| $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $1 / 2$ | $\begin{aligned} & 31 / 2 \\ & (89) \end{aligned}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{aligned} & 3,325 \\ & (14.8) \end{aligned}$ | $\begin{aligned} & 665 \\ & (3.0) \end{aligned}$ | $\begin{aligned} & 4,950 \\ & (22.0) \end{aligned}$ | $\begin{aligned} & 990 \\ & (4.4) \end{aligned}$ |
| $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | 5/8 | $\begin{gathered} 41 / 2 \\ (114) \end{gathered}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{aligned} & 3,850 \\ & (17.1) \end{aligned}$ | $\begin{array}{r} 770 \\ (3.4) \end{array}$ | $\begin{aligned} & 4,925 \\ & (21.9) \end{aligned}$ | $\begin{aligned} & 985 \\ & (4.4) \end{aligned}$ |
| $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $3 / 4$ | $\begin{gathered} 51 / 2 \\ (140) \end{gathered}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{aligned} & 5,200 \\ & (23.1) \end{aligned}$ | $\begin{gathered} 1,040 \\ (4.6) \end{gathered}$ | $\begin{aligned} & 4,450 \\ & (19.8) \end{aligned}$ | $\begin{aligned} & 890 \\ & (4.0) \end{aligned}$ |

1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
2. Values for 8 "-wide, medium-weight and normal-weight concrete masonry units.

For $3 / 8$ "- to $3 / 4$ "-diameter anchors, anchors may be installed in lightweight masonry units.
3. The masonry units must be fully grouted.
4. The minimum specified compressive strength of masonry, $\mathrm{f}^{\prime} m$, at 28 days is $2,000 \mathrm{psi}$.
5. Embedment depth is measured from the outside face of the concrete masonry unit.
6. Grout-filled CMU wall design must satisfy applicable design standards and be capable of withstanding applied loads.
7. Refer to allowable load-adjustment factors for spacing and edge distance on pp. 89-90.
8. Although the $1 / 4$ stainless steel Titen HD is not part of the evaluation report, we still tested the $1 / 4$ " screw per the appropriate AC.


Figure 1. Shaded Area = Placement for Full and Reduced Allowable Load Capacity in Grout-Filled CMU

## Stainless-Steel Titen HD ${ }^{\oplus}$ Design Information - Masonry

Stainless-Steel Titen HD Allowable Tension and Shear Loads in 8" Lightweight, Medium-Weight and Normal-Weight Hollow CMU

IBC


| $\begin{aligned} & \text { Size } \\ & \text { in. } \\ & (\mathrm{mm}) \end{aligned}$ | Drill Bit Diameter in. | Minimum Embedment Depth ${ }^{4}$ in. (mm) | $\begin{aligned} & \text { Critial } \\ & \text { Edge } \\ & \text { Distance } \\ & \text { in. } \\ & (\mathrm{mm}) \end{aligned}$ | Critical <br> Spacing Distance in. (mm) | 8" Hollow CMU Loads Based on CMU Strength |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Tension Load |  | Shear Load |  |
|  |  |  |  |  | Ultimate <br> lb. (kN) | Allowable <br> lb. (kN) | Ultimate lb. (kN) | Allowable <br> lb. (kN) |
| Anchor Installed in Face Shell (See Figure 2) |  |  |  |  |  |  |  |  |
| $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | 3/8 | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{aligned} & 925 \\ & (4.1) \end{aligned}$ | $\begin{aligned} & 185 \\ & (0.8) \end{aligned}$ | $\begin{aligned} & 2,250 \\ & (10.0) \end{aligned}$ | $\begin{aligned} & 450 \\ & (2.0) \end{aligned}$ |
| $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | 1/2 | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{gathered} 1,025 \\ (4.6) \end{gathered}$ | $\begin{aligned} & 205 \\ & (0.9) \end{aligned}$ | $\begin{aligned} & 2,325 \\ & (10.3) \end{aligned}$ | $\begin{aligned} & 465 \\ & (2.1) \end{aligned}$ |
| $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | 5/8 | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ | $\begin{aligned} & 550 \\ & (2.4) \end{aligned}$ | $\begin{array}{r} 110 \\ (0.5) \end{array}$ | $\begin{gathered} 2,025 \\ (9.0) \end{gathered}$ | $\begin{aligned} & 405 \\ & (1.8) \end{aligned}$ |
| $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $3 / 4$ | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 12 \\ (305) \end{gathered}$ | $\begin{gathered} \stackrel{8}{2} \\ (203) \end{gathered}$ | $\begin{aligned} & 775 \\ & (3.4) \end{aligned}$ | $\begin{array}{r} 155 \\ (0.7) \end{array}$ | $\begin{gathered} 1,975 \\ (8.8) \end{gathered}$ | $\begin{array}{r} 395 \\ (1.8) \end{array}$ |

1. The tabulated allowable loads are based on a safety factor of 5.0 for installations under the IBC and IRC.
2. Values for 8 "-wide, lightweight, medium-weight and normal-weight concrete masonry units.
3. The minimum specified compressive strength of masonry, $\mathrm{f}^{\prime} m$, at 28 days is $2,000 \mathrm{psi}$.
4. Embedment depth is measured from the outside face of the concrete masonry unit and is based on the anchor being embedded an additional $11 / 4$ "through $11 / 4$ "-thick face shell.
5. Allowable loads may not be increased for short-term loading due to wind or seismic forces. CMU wall design must satisfy applicable design standards and be capable of withstanding applied loads.
6. Do not use impact wrenches to install in hollow CMU.
7. Set drill to rotation-only mode when drilling into hollow CMU.
8. Refer to allowable load-adjustment factors for spacing and edge distance on p. 91.
9. Anchors must be installed a minimum of $11 / 2$ " from vertical head joints and $T$-joints. Refer to Figure 2 for permitted and prohibited anchor installation locations.


Figure 2. Stainless-Steel Titen HD Screw Anchor Installed in the Face of Hollow CMU Wall Construction

## Stainless-Steel Titen HD ${ }^{\oplus}$ Design Information - Masonry

Load-Adjustment Factors for Stainless-Steel Titen HD Anchors in Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

## How to use these charts:

1. The following tables are for reduced edge distance and spacing.
2. Locate the anchor size to be used for either a tension and/or shear load application.
3. Locate the embedment $(\mathrm{E})$ at which the anchor is to be installed.
4. Locate the edge distance ( $c_{\text {act }}$ ) or spacing (sact) at which the anchor is to be installed.
5. The load adjustment factor ( $f_{c}$ or $f_{s}$ ) is the intersection of the row and column.
6. Multiply the allowable load by the applicable load adjustment factor.
7. Reduction factors for multiple edges or spacings are multiplied together.


| $\begin{aligned} & c_{\text {act }} \\ & \text { (in.) } \end{aligned}$ | Dia. | 1/4 | $3 / 8$ | 1/2 | 5/8 | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | 2112 | 23/4 | $31 / 2$ | $41 / 2$ | $51 / 2$ |
|  | $c_{c r}$ | 4 | 12 | 12 | 12 | 12 |
|  | $c_{\text {min }}$ | 1.25 | 4 | 4 | 4 | 4 |
|  | $f_{c \text { min }}$ | 0.84 | 0.80 | 0.81 | 1.00 | 1.00 |
| 1.25 |  | 0.84 |  |  |  |  |
| 2 |  | 0.88 |  |  |  |  |
| 3 |  | 0.94 |  |  |  |  |
| 4 |  | 1.00 | 0.80 | 0.81 | 1.00 | 1.00 |
| 6 |  | 1.00 | 0.85 | 0.86 | 1.00 | 1.00 |
| 8 |  | 1.00 | 0.90 | 0.91 | 1.00 | 1.00 |
| 10 |  | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 |
| 12 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

See footnotes below.
Edge Distance Shear ( $\mathrm{f}_{\mathrm{c}}$ )
Shear Load Parallel to Edge or End
IBC


| $\mathrm{C}_{\text {act }}$ <br> (in.) | Dia. | $1 / 4$ | 3/8 | 1/2 | 5/8 | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | $23 / 4$ | $31 / 2$ | $41 / 2$ | $51 / 2$ |
|  | $c_{c r}$ | 4 | 12 | 12 | 12 | 12 |
|  | $c_{\text {min }}$ | 1.25 | 4 | 4 | 4 | 4 |
|  | $f_{c m i n}$ | 0.89 | 0.88 | 0.56 | 0.65 | 0.84 |
| 1.25 |  | 0.89 |  |  |  |  |
| 2 |  | 0.92 |  |  |  |  |
| 3 |  | 0.96 |  |  |  |  |
| 4 |  | 1.00 | 0.88 | 0.56 | 0.65 | 0.84 |
| 6 |  | 1.00 | 0.91 | 0.67 | 0.74 | 0.88 |
| 8 |  | 1.00 | 0.94 | 0.78 | 0.83 | 0.92 |
| 10 |  | 1.00 | 0.97 | 0.89 | 0.91 | 0.96 |
| 12 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

See footnotes below.
Edge Distance Shear ( $\mathrm{f}_{\mathrm{c}}$ )
Shear Load Perpendicular to Edge or End (Directed Towards Edge or End)

IBC


| $\begin{aligned} & \mathrm{C}_{\text {act }} \\ & \text { (in.) } \end{aligned}$ | Dia. | $1 / 4$ | 3/8 | $1 / 2$ | 5/8 | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | 21/2 | $23 / 4$ | $31 / 2$ | $41 / 2$ | $51 / 2$ |
|  | $C_{c r}$ | 4 | 12 | 12 | 12 | 12 |
|  | $c_{\text {min }}$ | 1.25 | 4 | 4 | 4 | 4 |
|  | $f_{c m i n}$ | 0.33 | 0.93 | 0.48 | 0.66 | 0.69 |
| 1.25 |  | 0.33 |  |  |  |  |
| 2 |  | 0.51 |  |  |  |  |
| 3 |  | 0.76 |  |  |  |  |
| 4 |  | 1.00 | 0.93 | 0.48 | 0.66 | 0.69 |
| 6 |  | 1.00 | 0.95 | 0.61 | 0.75 | 0.77 |
| 8 |  | 1.00 | 0.97 | 0.74 | 0.83 | 0.85 |
| 10 |  | 1.00 | 0.98 | 0.87 | 0.92 | 0.92 |
| 12 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

1. $E=$ embedment depth (inches).
2. $c_{\text {act }}=$ actual end or edge distance at which anchor is installed (inches).
3. $c_{c r}=$ critical end or edge distance for $100 \%$ load (inches).
4. $c_{\text {min }}=$ minimum end or edge distance for reduced load (inches).
5. $f_{C}=$ adjustment factor for allowable load at actual end or edge distance.
6. $f_{c c r}=$ adjustment factor for allowable load at critical end or edge distance. $f_{c c r}$ is always $=1.00$.
7. $f_{c \text { min }}=$ adjustment factor for allowable load at minimum end or edge distance.
8. $f_{c}=f_{c \text { min }}+\left[\left(1-f_{\text {cmin }}\right)\left(c_{\text {act }}-c_{\text {min }}\right) /\left(c_{c r}-c_{\text {min }}\right)\right]$.

Load-Adjustment Factors for Stainless-Steel Titen HD Anchors in Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads (cont.)

## How to use these charts:

1. The following tables are for reduced edge distance and spacing.
2. Locate the anchor size to be used for either a tension and/or shear load application.
3. Locate the embedment (E) at which the anchor is to be installed.
4. Locate the edge distance ( $c_{\text {act }}$ ) or spacing ( $S_{\text {act }}$ ) at which the anchor is to be installed.
5. The load adjustment factor $\left(f_{c}\right.$ or $\left.f_{s}\right)$ is the intersection of the row and column.
6. Multiply the allowable load by the applicable load adjustment factor.
7. Reduction factors for multiple edges or spacings are multiplied together.

Edge Distance Shear ( $\mathrm{f}_{\mathrm{c}}$ )
Shear Load Perpendicular to Edge or End IBC
(Directed Away from Edge or End)

| $\mathrm{C}_{\text {act }}$ <br> (in.) | Dia. | $1 / 4$ | 3/8 | 1/2 | 5/8 | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | 23/4 | $31 / 2$ | $41 / 2$ | $51 / 2$ |
|  | $c_{c r}$ | 4 | 12 | 12 | 12 | 12 |
|  | $c_{\text {min }}$ | 1.25 | 4 | 4 | 4 | 4 |
|  | $f_{\text {cmin }}$ | 0.33 | 0.93 | 0.48 | 0.66 | 0.69 |
| 1.25 |  | 0.33 |  |  |  |  |
| 2 |  | 0.51 |  |  |  |  |
| 3 |  | 0.76 |  |  |  |  |
| 4 |  | 1.00 | 0.93 | 0.48 | 0.66 | 0.69 |
| 6 |  | 1.00 | 0.95 | 0.61 | 0.75 | 0.77 |
| 8 |  | 1.00 | 0.97 | 0.74 | 0.83 | 0.85 |
| 10 |  | 1.00 | 0.98 | 0.87 | 0.92 | 0.92 |
| 12 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

Spacing Tension $\left(\mathrm{f}_{\mathrm{s}}\right)$
IBC 苗 国

| $\begin{aligned} & \text { Sact } \\ & \text { (in.) } \end{aligned}$ | Dia. | 1/4 | $3 / 8$ | 1/2 | 5/8 | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | 2112 | $23 / 4$ | $31 / 2$ | $41 / 2$ | $51 / 2$ |
|  | $S_{\text {cr }}$ | 4 | 8 | 8 | 8 | 8 |
|  | $s_{\text {min }}$ | 2 | 4 | 4 | 4 | 4 |
|  | $\mathrm{f}_{\text {smin }}$ | 0.79 | 0.81 | 0.79 | 0.87 | 0.78 |
| 2 |  | 0.79 |  |  |  |  |
| 3 |  | 0.90 |  |  |  |  |
| 4 |  | 1.00 | 0.81 | 0.79 | 0.87 | 0.78 |
| 6 |  |  | 0.91 | 0.90 | 0.94 | 0.89 |
| 8 |  |  | 1.00 | 1.00 | 1.00 | 1.00 |

Spacing Shear ( $\mathrm{f}_{\mathrm{s}}$ )


| $\begin{aligned} & \text { Sact } \\ & \text { (in.) } \end{aligned}$ | Dia. | $1 / 4$ | 3/8 | 1/2 | 5/8 | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | 21/2 | $23 / 4$ | $31 / 2$ | $41 / 2$ | $51 / 2$ |
|  | $s_{c r}$ | 4 | 6 | 8 | 10 | 12 |
|  | $s_{\text {min }}$ | 2 | 3 | 4 | 5 | 6 |
|  | $\mathrm{f}_{\text {smin }}$ | 0.78 | 1.00 | 0.86 | 0.90 | 0.94 |
| 2 |  | 0.78 |  |  |  |  |
| 3 |  | 0.89 |  |  |  |  |
| 4 |  | 1.00 | 1.00 | 0.86 | 0.90 | 0.94 |
| 6 |  |  | 1.00 | 0.93 | 0.95 | 0.97 |
| 8 |  |  | 1.00 | 1.00 | 1.00 | 1.00 |

1. $\mathrm{E}=$ embedment depth (inches).
2. $s_{\text {act }}=$ actual spacing distance at which anchors are installed (inches).
3. $s_{c r}=$ critical spacing distance for $100 \%$ load (inches).
4. $s_{\text {min }}=$ minimum spacing distance for reduced load (inches).
5. $\mathrm{f}_{s}=$ adjustment factor for allowable load at actual spacing distance.
6. $\mathrm{f}_{\text {scr }}=$ adjustment factor for allowable load at critical spacing distance. $\mathrm{f}_{\text {scr }}$ is always $=1.00$.
7. $\mathrm{f}_{\text {smin }}=$ adjustment factor for allowable load at minimum spacing distance.
8. $f_{s}=f_{\text {smin }}+\left[\left(1-f_{\text {smin }}\right)\left(s_{\text {act }}-s_{\text {min }}\right) /\left(s_{c r}-s_{\text {min }}\right)\right]$.

## Stainless-Steel Titen HD ${ }^{\oplus}$ Design Information - Masonry

Load-Adjustment Factors for Stainless-Steel Titen HD Anchors in Face-of-Wall Installation in 8" Hollow CMU: Edge Distance and Spacing, Tension and Shear Loads

## How to use these charts:

1. The following tables are for reduced edge distance and spacing.
2. Locate the anchor size to be used for either a tension and/or shear load application.
3. Locate the embedment (E) at which the anchor is to be installed.
4. Locate the edge distance ( $c_{a c t}$ ) or spacing ( $s_{\text {act }}$ ) at which the anchor is to be installed.

## Edge Distance Tension ( $\mathrm{f}_{\mathrm{c}}$ )

| $\begin{aligned} & C_{\text {act }} \\ & \text { (in.) } \end{aligned}$ | Dia. | $3 / 8$ | 1/2 | 5/8 | $3 / 4$ | IBC ${ }^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | $21 / 2$ | 2112 | $21 / 2$ |  |
|  | $C_{c r}$ | 12 | 12 | 12 | 12 | - |
|  | $c_{\text {min }}$ | 4 | 4 | 4 | 4 | 8 |
|  | $f_{c m i n}$ | 1.00 | 1.00 | 1.00 | 1.00 | W |
| 4 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| 6 |  | 1.00 | 1.00 | 1.00 | 1.00 | $\mathrm{Cl}_{0}^{0}$ |
| 8 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| 10 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| 12 |  | 1.00 | 1.00 | 1.00 | 1.00 |  |

1. $E=$ embedment depth (inches).
2. $c_{\text {act }}=$ actual end or edge distance at which anchor is installed (inches).
3. $c_{c r}=$ critical end or edge distance for $100 \%$ load (inches).
4. $c_{\text {min }}=$ minimum end or edge distance for reduced load (inches).
5. $f_{C}=$ adjustment factor for allowable load at actual end or edge distance.
6. $f_{c c r}=$ adjustment factor for allowable load at critical end or edge distance. $\mathrm{f}_{\mathrm{Cc}}$ is always $=1.00$.
7. $\mathrm{f}_{\text {cmin }}=$ adjustment factor for allowable load at minimum end or edge distance.
8. $f_{c}=f_{c \text { min }}+\left[\left(1-f_{c \text { min }}\right)\left(c_{a c t}-c_{\text {min }}\right) /\left(c_{c r}-c_{\text {min }}\right)\right]$.

## Spacing Tension ( $\mathrm{f}_{\mathrm{s}}$ )

One Anchor per Cell

| $\begin{aligned} & \mathrm{C}_{\text {act }} \\ & \text { (in.) } \end{aligned}$ | Dia. | 3/8 | 1/2 | 5/8 | $3 / 4$ | IBC ${ }^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | $21 / 2$ | $21 / 2$ | $21 / 2$ |  |
|  | $c_{c r}$ | 8 | 8 | 8 | 8 | , |
|  | $c_{\text {min }}$ | 4 | 4 | 4 | 4 | 3 |
|  | $f_{c \text { min }}$ | 0.72 | 0.87 | 0.89 | 0.70 | 20] |
| 4 |  | 0.72 | 0.87 | 0.89 | 0.70 |  |
| 6 |  | 0.86 | 0.94 | 0.95 | 0.85 |  |
| 8 |  | 1.00 | 1.00 | 1.00 | 1.00 | $\longleftrightarrow$ |

See notes below.

Spacing Shear ( $\mathrm{f}_{\mathrm{s}}$ )
One Anchor per Cell

| Sact <br> (in.) | Dia. | 3/8 | 1/2 | 5/8 | 3/4 | IBC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | $21 / 2$ | $21 / 2$ | $21 / 2$ |  |
|  | $s_{c r}$ | 8 | 8 | 8 | 8 |  |
|  | $s_{\text {min }}$ | 4 | 4 | 4 | 4 | 3 |
|  | $\mathrm{f}_{\text {smin }}$ | 0.81 | 1.00 | 0.71 | 0.74 | 2 |
| 4 |  | 0.81 | 1.00 | 0.71 | 0.74 | $\square$ |
| 6 |  | 0.91 | 1.00 | 0.86 | 0.87 | -0 |
| 8 |  | 1.00 | 1.00 | 1.00 | 1.00 | $\leftrightarrow$ |

1. $E=$ embedment depth (inches).
2. $s_{\text {act }}=$ actual spacing distance at which anchors are installed (inches).
3. $s_{c r}=$ critical spacing distance for $100 \%$ load (inches).
4. $s_{\text {min }}=$ minimum spacing distance for reduced load (inches).
5. $\mathrm{f}_{S}=$ adjustment factor for allowable load at actual spacing distance.
6. $\mathrm{f}_{\text {scr }}=$ adjustment factor for allowable load at critical spacing distance. $\mathrm{f}_{\text {scr }}$ is always $=1.00$.
7. $f_{\text {smin }}=$ adjustment factor for allowable load at minimum spacing distance.
8. $f_{s}=f_{\text {smin }}+\left[\left(1-f_{\text {smin }}\right)\left(s_{\text {act }}-s_{\text {min }}\right) /\left(s_{c r}-s_{\text {min }}\right)\right]$.
9. The load adjustment factor $\left(f_{C}\right.$ or $\left.f_{S}\right)$ is the intersection of the row and column.
10. Multiply the allowable load by the applicable load adjustment factor.
11. Reduction factors for multiple edges or spacings are multiplied together.

Edge Distance Shear ( $\mathrm{f}_{\mathrm{c}}$ )

| $*$ <br> $\boldsymbol{c}_{\text {act }}$ <br>  | Dia. | $3 / 8$ | $1 / 2$ | $5 / 8$ | $3 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | $21 / 2$ | $21 / 2$ | $21 / 2$ |
|  | $c_{\text {cr }}$ | 12 | 12 | 12 | 12 |
|  | $c_{\text {min }}$ | 4 | 4 | 4 | 4 |
|  | $f_{\text {cmin }}$ | 0.78 | 0.63 | 0.55 | 0.51 |
| 4 |  | 0.78 | 0.63 | 0.55 | 0.51 |
| 6 |  | 0.84 | 0.72 | 0.66 | 0.63 |
| 8 |  | 0.89 | 0.82 | 0.78 | 0.76 |
| 10 |  | 0.95 | 0.91 | 0.89 | 0.88 |
| 12 |  | 1.00 | 1.00 | 1.00 | 1.00 |

Spacing Tension ( $\mathrm{f}_{\mathrm{s}}$ )
Two Anchors per Cell

| $\begin{aligned} & \text { cart } \\ & \text { (in.) } \end{aligned}$ | Dia. | $3 / 8$ | 1/2 | 5/8 | $3 / 4$ | IBC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E | $21 / 2$ | $21 / 2$ | $21 / 2$ | $21 / 2$ |  |
|  | $c_{c r}$ | 8 | 8 | 8 | 8 | T |
|  | $c_{\text {min }}$ | 4 | 4 | 4 | 4 | 0 |
|  | $f_{\text {cmin }}$ | 1.00 | 1.00 | 1.00 | 0.78 |  |
| 4 |  | 1.00 | 1.00 | 1.00 | 0.78 | $\underline{\square}$ |
| 6 |  | 1.00 | 1.00 | 1.00 | 0.89 |  |
| 8 |  | 1.00 | 1.00 | 1.00 | 1.00 | $\xrightarrow{5}$ |

See notes below.

Spacing Shear ( $\mathrm{f}_{\mathrm{s}}$ )
Two Anchors per Cell



[^0]:    Suggested fixture hole sizes are for structural steel thicker than 12 gauge only. Larger holes are not required for wood or thinner cold-formed steel members.

[^1]:    $\dagger$ These models do not meet minimum embedment depth requirements for strength design and require maximum installation torque of 25 ft . lb . using a torque wrench, driver drill or cordless $1 / 4 "$ impact driver with a maximum permitted torque rating of 100 ft . lb .

    1. Anchor length is measured from top of head to bottom of anchor.
